# THE IDENTIFICATION AND TESTING OF GROUNDWATER SOURCES FOR COMMUNAL WATER SUPPLY VILLAGE OF VARS, ONTARIO

PRELIMINARY DRAFT
(FOR DISCUSSION PURPOSES ONLY)

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#### 1.0 INTRODUCTION

Water and Earth Science Associates Limited was contracted by McNeely Engineering Limited on behalf of the Township of Cumberland to conduct a water supply source identification study and testing program for a communal water supply development for the Village of Vars. Background research of MOE well records and the geological literature had identified a glaciofluvial complex located approximately 3 kilometers east of the village as a likely target area (Figure 1).

Work on Vars water supply project has spanned a 4 year period. As indicated in Table 1, Phase 1 of the investigation consisted of a background study and mapping program, while Phase II consisted of a more detailed testing program. Phase III involved the water treatability study.

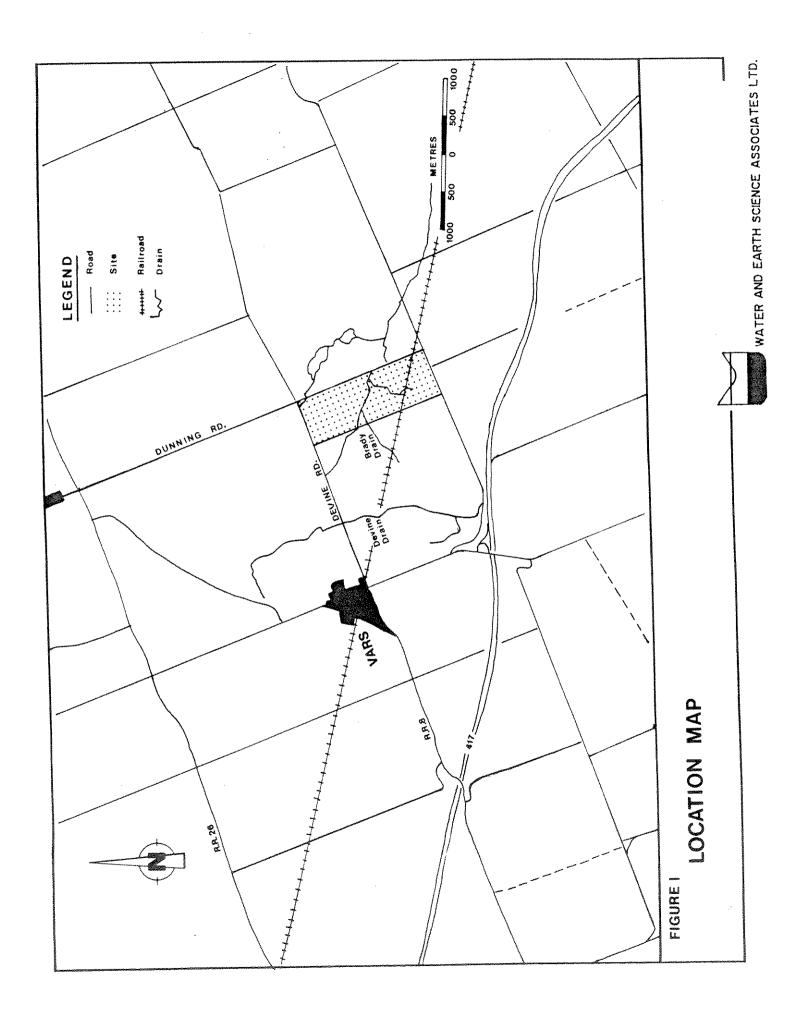
#### TABLE 1: VARS WATER SUPPLY STUDY

- Phase I Water supply source identification 1986
  (Background study)
  Source investigation and testing 1986-87
  (Mapping program)
- Phase IIa Source quantification and testing 1987 (Test well program)
- Phase IIb Water Quality Verification Testing 1990 (Test well program)
- Phase III Water supply treatability study 1990

This report presents the results of the first two phases of the program. Phase III can be found under a separate cover (WESA, 1990b).

#### 2.0 METHODS OF ANALYSIS

During Phase I, potential aquifer sites which were identified during the background research and the site reconnaissance, were investigated through a geological and hydrogeological mapping program of these sites. Preliminary mapping of the Cumberland Township included observation of natural and man-made exposures in gravel pits and river banks located along the glaciofluvial complex. As most farms and residences along the glaciofluvial complex rely on shallow dug wells which are not usually recorded in MOE well log files, well log information in these areas was largely unavailable. Stereo air photographs were examined to determine the location and width of the glaciofluvial deposits identified as the prime drilling



targets for water supply development on a communal scale. The results of a geophysical survey completed by the Ministry of Natural Resources were reviewed as were the internal WESA files detailing the morphology, location and orientation of the esker sand and gravel deposits in Eastern Ontario. Valuable unpublished information was also obtained from representatives of the MNR regarding the location of the buried glaciofluvial deposits in the area (Gorrell, 1987).

During the reconnaissance mapping program, eighty-six test holes were drilled, by either a truck mounted CME 75 or a track mounted CME 55 hollowstem drill rig. The reconnaissance drilling program covered most of the countryside east and north of Vars towards Leonard, Ontario. The program was successful in identifying a number of target locations. The screening criteria used in this identification included: the permeability of the deposit, the thickness of the saturated deposit, the recharge potential of the site, the proximity and character of potential contaminant sources, and the pipe line distance to Vars.

Samples of the unconsolidated surficial materials drilled were obtained by split spoon sampler test holes for later examination.

Selected drill holes were instrumented with piezometers for later use as hydraulic head monitors. Geologic, hydrogeologic and instrumentation details are compiled in Appendix A. The locations of the test holes and the piezometers are shown on Figure 2.

Geologic information was compiled in the form of crosssections, isopach thickness maps, and test hole logs. After the completion of a level survey, the exact locations and actual elevation of the tops of the piezometer casings were determined and tied together to a common datum.

Hydraulic heads were obtained from the piezometer network to establish natural groundwater gradient fields and the recharge/discharge regime of the glaciofluvial complex was determined.

An initial potential water supply location was identified 7.5 km south of Leonard, Ontario. However, the expense of piping the water to Vars warranted further investigation closer to Vars. A small area just southwest of Vars was investigated in early March of 1987 with no success.

In late 1987, new geophysical information was provided by the Ministry of Natural Resources which showed that a very narrow extension of the glaciofluvial deposit was located south of the Devine Road and east of Vars. This area was test drilled in May and June of 1987.

The Phase IIa study included the determination of the optimum location and design of a 200 mm (nominal 8 inch) diameter naturally gravel packed test well capable of producing a minimum of 7.6 - 11.4 l/s (100-150 IGPM) of potable water. The optimal location was optioned by the Township of Cumberland prior to testing. The well was installed and tested for yield, efficiency, and water quality. Interference effects and a long term appraisal of safe perennial yield, recharge, and water quality were also calculated. The Test Well 1 site was located close to the Devine Road. This site was chosen for its potential to provide substantial yield without interfering with the neighbouring domestic and agricultural water supplies.

The test well was installed by Olympic Drilling Co. Ltd. a local drilling contractor with considerable experience in large scale water supply well drilling. A 29T cable tool drill rig was used to install the well to a depth of 22.25 metres (73 feet). A 200 mm telescoping stainless steel wire wrap screen was installed by the pull-back method. The interval from 18.28 metres to 20.73 metres (60 to 68 feet) below ground surface was The screen was designed during the drilling and included analyses of the grain size distribution of the aquifer materials by a suction bailer. A #100 slot size screen opening was selected. The test well configuration is as shown on Figure This test well was designed so that if successful it could be used as a standby pumping facility at a later date with minor modification. If unsuccessful, the stainless steel screen could be recovered.

After drilling, the well was developed by compressed air surging and over pumping with the shaft line turbine pump installed for testing purposes. The well was developed until essentially sand free.

The aquifer testing program undertaken included an initial step discharge pumping test. The well was pumped incrementally at discharges of 7.58 l/s, 15.15 l/s, 30.30 l/s, 38.86 l/s (100 IGPM, 200 IGPM, 300 IGPM, 400 IGPM, 513 IGPM) for periods up to 30 minutes each. Discharge was measured with an orifice weir and manometer. Test data can be found in Appendix B. Pumped water from all testing was discharged through a 300 foot pipeline into the bush northeast of the test well. A deposit of clay and silt up to 6 metres thick overlies and hydraulically isolates the aquifer from surface infiltration at this location. Drainage of the water is away from the crest of the aquifer.

A constant discharge aquifer test was conducted at the conclusion of recovery of water levels after the step discharge test. The aquifer test spanned a period of 72 hours and a

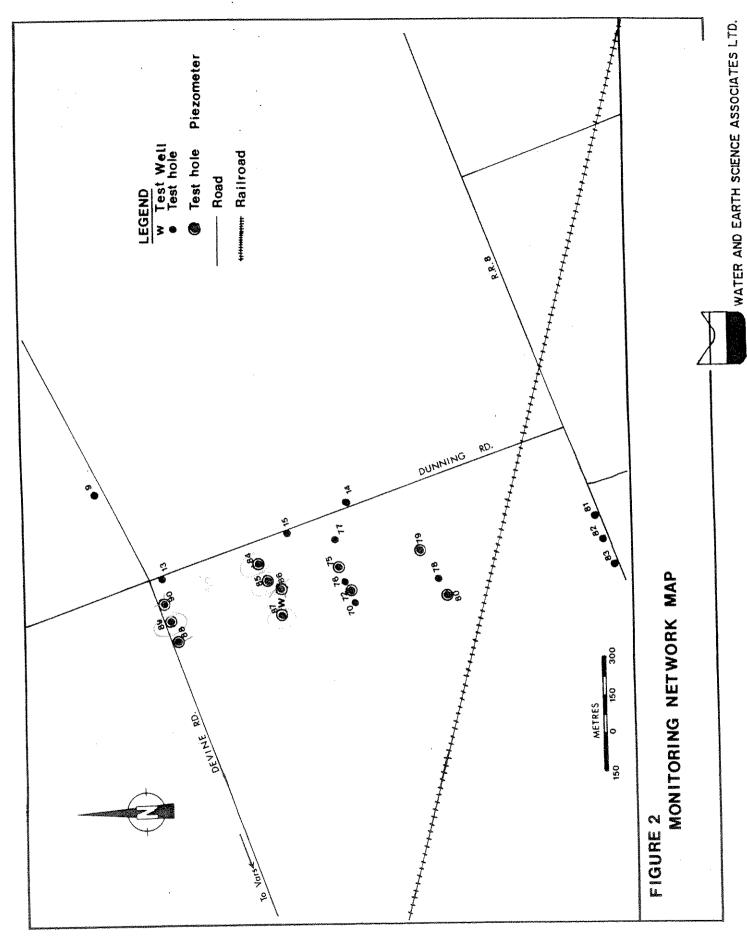


FIGURE	3	RECORD OF TEST HOLE			GNATION W1		COMPLETION DATE September 25, 1987			
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— 10 <b>.</b> 97—	_	CLAY AND GRAVEL - granule and pebble gravel with silt and clay matrix; minor sand	0,00						Sample 3 Sample 4	
		GRAVEL - coarse grained sand, loosely	5 0 p						Sample S	
- 12		packed with granule and pebble sized gravel	One						- Sample 6	12.2 m
		(rounded to subrounded).  At 11.9-12.2 m cobble sized gravel is	000						Sample 7	1
_ 14		encountered; silty matrix near top of		d l					Sample 8	14.6 m
		gravel, gradually silt matrix decreases with	800						Sample 9	15.4 m
- 16		depth	P4.9.0		20 cm					
			0.00		(811)				Sample 10 Sample 11	16.76m
12			0.00	q					Батр1е1 <u>2</u>	1
18 18.28 —	<del> </del>	GRAVEL - granules and very coarse grained	13:0°C	4	2000	2 4 m	(8') of			
		sand with rounded to subrounded pebbles and cobbles (10-12 cm in diameter). No	000			100 slo			Sample 13	19.8 m
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constant discharge of 26.5 l/s (350 IGPM) was maintained throughout. The drawdown of piezometric levels in the pumping well and 11 monitors was measured by means of an electric tape.

The recovery of the system was continually monitored for 24 hours after the pump was shut down. Water levels were checked once more at the 42 hour mark after the pump was shut off. The drawdown and recovery data are contained in Appendix C-1.

The chemical and bacteriological quality of the water was monitored during the course of the constant discharge aquifer test. Samples were obtained at regular intervals by established protocols. Samples for bacterial analysis were submitted to Kopp Labs of Ottawa and the Ministry of Health Laboratory. Samples for chemical analyses were submitted to Bondar-Clegg and Company of Ottawa. Other water quality parameters such as pesticides, herbicides, PCB, volatile organics GC/MS (US EPA 624) and total phenolics were analysed by Mann Testing Inc. of Mississauga Ontario. Completed analytical reports are contained in Appendix D-1.

A draft report was prepared and submitted in 1987 to the M.O.E. Regional office in Kingston for review.

Work on this project was reinitiated in April 1990 at the request of McNeely Engineering Ltd. Phase IIb of the study involved the re-pumping of the water supply test well to collect water samples for the treatability test program and to address water quality concerns identified by the Ontario Ministry of the Environment (MOE) in their report review dated March 23, 1988 and in telephone conversations with the M.O.E. Regional office in Kingston in May of 1990 (pers. comm. Mr. Frank Crossley, see Appendix E).

In May 1990 the test well was pumped at the design discharge of 26.5 l/s (350 IGPM) for a period of 72 hours. The drawdown of piezometric levels in the aquifer was measured with an electric tape in the pumping well and four of the monitoring piezometers. Physical analysis of the retest was restricted to a brief comparison between the 1987 and the 1990 data and was completed to ensure consistency in the performance of the aquifer (drawdown data are contained in Appendix C-2).

A strict quality assurance and quality control (QA/QC) program was followed during this phase of sampling to alleviate difficulties previously observed in the water quality data. A submersible pump was used for pumping the well. All equipment was precleaned before installation. Teflon tape was used on all connecting joints of the discharge pipe. Duplicate samples were collected at each sampling interval and triples were collected at the 72 hr interval. All bottles and caps were rinsed 6x with

sample water before the sample was collected. All samples requiring pretreatment were prepared under controlled conditions the laboratory. A complete analytical suite as stipulated on Tables 1, 1A, 2, and 3 (MOE, 1984) were undertaken with a number of additions. In addition to the analysis of trihalomethanes, as required by the MOE, additional analyses for volatile organic compounds (VOC) were undertaken. The USEPA 624 sampling and analytical protocol was followed for the VOC's.

One complete suite of analyses, including VOC's, were provided by Areco Canada Inc. of Nepean, Ontario. Interlaboratory quality control checks were conducted on duplicate samples taken at the 72 hr sampling episode for Ur, Fe, colour, turbidity, TOC, bacti, phenol and analyzed at Accutest Laboratories of Nepean. A duplicate VOC sample was sent to Novalab in Lachine Quebec. Travel blanks were prepared and shipped with all samples. Complete analytical reports are contained in Appendix D-2.

#### 3.0 RESULTS

#### 3.1 Topography and Drainage

The glaciofluvial complex in the study area is completely buried in most areas, and has no surface relief except near testhole 78, where a slight rise is noted. Where the sands and gravels reach the surface along the crest of the deposit, recharging precipitation is able to infiltrate rapidly into the underlying permeable formation. However, most of the sands and gravels (on the flanks) are overlain by a clayey silt unit and prevents infiltration of precipitation. The glacial fluvial deposit is drained on its western edge by the north/south oriented Devine Drain. The Brady drainage ditch cuts across the study site about midway between the Devine Rd. and Regional Road # 8 at test wells 70 and 71 and appears to flow southeast. A second ditch begins on the southwest side of the complex and cuts northeastward to the deposits eastern edge near the road.

#### 3.2 Geology

The study area is underlain by Paleozoic bedrock of the upper Ordovician period described by Wilson (1946) as the Carlsbad Formation. The formation consists of layered bioclastic limestone which is medium grey colour on freshly broken surfaces and buff to reddish brown on a weathered surface.

The water in this unit is characteristically sulphurous and exhibits elevated concentrations of iron.

The bedrock in the study area is overlaid by a succession of Wisconsinian Epoch glacial, glaciofluvial and glaciomarine unconsolidated sediments. A clayey sandy, calcarious compact till directly overlies the bedrock throughout the study area. This unit is fairly thin, with the maximum thickness of 1.6 m at test well 72.

Melt water derived glaciofluvial deposits were deposited by the receding glacial ice. These deposits are oriented north-south and appear as esker and buried esker morphologies at at least five locations in this part of the province. deposits are being utilized or are destined to be used as municipal water supplies at at least four locations in eastern Ontario. The Vars study area lies on one such esker deposit which is believed to be a continuation of the same unit identified at Sarsfield and Leonard, and it appears to extend across the Highway 417 into the County of Russell. The water supplies for the municipalities of Embrun and Chesterville are developed into this unit to the south. The distances between the centres of pumping of these water supplies are large enough that interference is not considered to be an issue. The complex varies between 15.2 m and 30.5 m in width, and has an average thickness of 23.8 m in the study area.

The esker body appears to be coarser grained along the main axis but shows significant but less transmissive connection to sand deposits flanking the main core or axis of the deposit. The most transmissive part of the water bearing unit appears to have an average saturated thickness of 13 m. The deposit reached its maximum thickness near the test hole, at 21.6 m (78 ft). The base of the unit lies on a relatively impermeable basal till. The upper surface of the esker outcrops in only a few places and is usually covered by a clayey silt unit. This impermeable unit acts as a barrier to surface contamination, yet also results in reduced recharge capabilities.

The esker is bounded on both sides by a silty glaciomarine clay deposit of Champlain Sea origin. This unit characteristically has a low permeability. The entire complex is overlain by a variable thickness of fine to medium grained silty sand. This is described as a regressive sequence by Terasmae (1965) and is made up of material derived from higher topographic sites in the area through water washing and winnowing by the Champlain Sea. The sand reaches a thickness of up to 5.5 m at test hole 87 on the Bray property.

#### 3.3 Physical Hydrogeology

The background geological and hydrogeological appraisal (Phase 1 Activities) identified two areas with water supply potential. Both of these areas were located in the glaciofluvial deposits east of Vars. The deposit to the southeast of the

village and south of the Devine road was selected as the primary drilling target for Phase 2, the detailed hydrogeological assessment.

#### 3.3.1 Test Drilling

Test drilling results indicated that a narrow 15 to 30 metre wide body of esker sands and gravels were present south of the Devine Road approximately 3 km east of the village of vars (Figure 2). The narrow width of the deposit was compensated for by a significant thickness on the order of 20 metres at the proposed test well site. The sands and gravels outcrop along the axis of the esker and thereby present some significant recharge potential especially to the north of the proposed test well site.

The core of the esker body provides a high transmissivity pathway for recharge derived from areas to the north and south of the test well site. The less permeable sands flanking the main esker body serve as recharge and storage reservoirs for the system. A plot of the thickness of the water bearing deposit is shown in Figure 4.

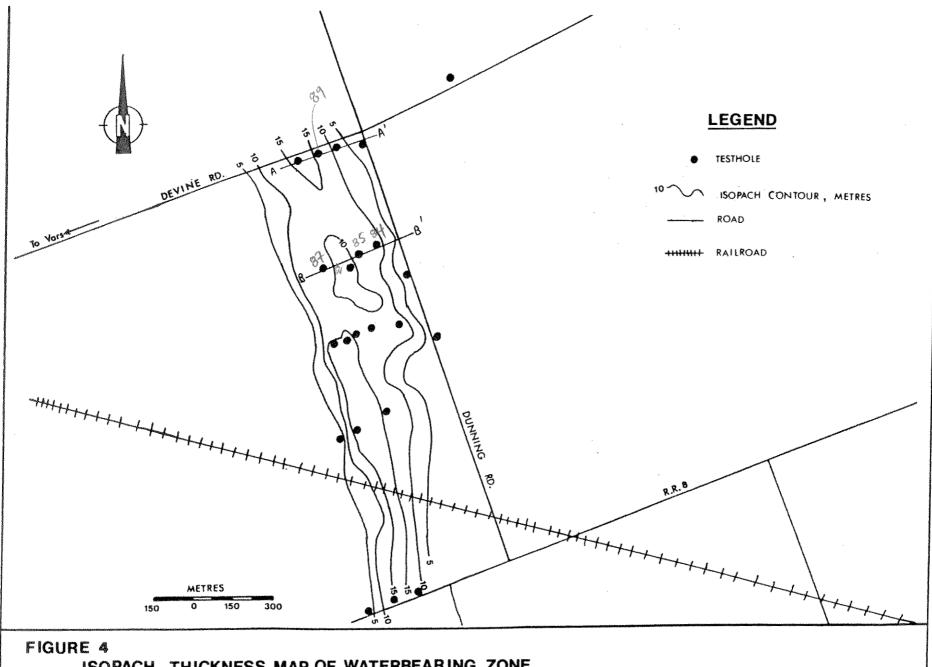
#### 3.3.2 Aguifer Testing - 1987 Program

#### Step Discharge Test

The results of the five step, step discharge test indicate that the test well, although not particularly efficient, was capable of producing test flows in excess of the proposed design flow of 11.3 1/s (150 IGPM). Data and calculations after Jacob-Rorabough are contained in Appendix B. Results of this imperial method were unsatisfactory at a discharge of 26.51 1/s (350 IGPM). An efficiency of 5.5 % was calculated for a discharge of 26.51 1/s. This does not correspond to the observed drawdown or the efficiency calculated by other more direct means. A calculation of well efficiency obtained from a comparison of the theoretical versus the actual drawdown yielded an efficiency of 37.7 % at a discharge of 26.51 1/s at 72 hours. This value is also believed to be very conservative given the bounded nature of the aguifer.

#### Constant Discharge Aguifer Test

The test well was pumped at a discharge of 26.51 1/s (350 IGPM) for a period of 72 hours. Data and Calculations are contained in Appendix C. Results of calculations of the aquifer hydraulic parameters are contained on Table 2.



ISOPACH THICKNESS MAP OF WATERBEARING ZONE



TABLE 2: AOUIFER PARAMETER SUMMARY

	radial distance		Transmissivities (m <sup>2</sup> /day)				
	from pumping	Jacob	Jacob	Jacob			
	well (m)	Drawdown	Recovery	<u>Drawdown</u>			
TW1	0.1	806.4	1233.3				
TH87	3.5	822.2	1148.8	11.8			
P72	277.5	1326.9	901.8	$5.25 \times 10^{-3}$			
P88	435	1075.0		$1.09 \times 10^{-2}$			
P89	450	814.2	1198.0	1.38 X 10 <sup>-3</sup>			
P80	667	814.2	1270.6	$1.6 \times 10^{-3}$			

Examination of the drawdown curves and the calculated storativities indicates that the aquifer behaves hydraulically as a confined unit with significant negative boundary conditions. The boundary condition effects are most likely felt in very early time given the high transmissivities found in the aquifer core and the short distances present. Calculated storativities on the order of 1.5 X 10-3 appear to be representative. Measurable drawdowns were recorded in piezometers at large radial distances from the pumping well immediately after the start of pumping. This is indicative of a high transmissivity medium. response of the piezometers located outside of the highly transmissive core of the esker is slower but non the less shows hydraulic connection to the core. This connection is delayed, and in the case of the transition from pumping to recovery the heads in these piezometers never do catch up to the drawdown in piezometers developed into the transmissive core of the deposit. A transmissivity on the order of 1000 m2/day was calculated for the transmissive core of the esker deposit, and used for later calculation of long term yield and well interference.

#### Aquifer Recovery Test

Water levels were observed and recorded for a 24 hour period at the conclusion of the 72 hours of continuous pumping of the aquifer. The same observation points as those used during pumping were employed. Heads in the aquifer recovered in the vicinity of the test well to within 0.5 metres of the original static condition with in this time period. Recovery in the piezometers located off the axis of the esker showed either no recovery or a recovery that was time lagged. This was in response to a transient head condition in the less permeable deposits during the latter stages of pumping and continued drawdown in these materials during recovery. transmissivities calculated from the recovery data are significantly higher that those derived from the drawdown test in the pumping well. This discrepancy is attributed to the effects

of well efficiency. The recovery data also exhibits less influence from the negative boundary conditions experienced during the pumping phase of the program.

#### 3.3.3 Aquifer Testing - 1990 Program

The static measurements in the pumping well and the four observation wells were recorded prior to the start-up of the pumping test. The step test and recovery test was not repeated. A monitoring program consistent with the previous testing interval was established in the pumping well during the continuous discharge test. Observation wells were monitored at regular intervals. The results can be found in Appendix C-2. Table 3 is a summary of the physical test data.

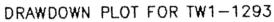
TABLE 3: 1990 DISCHARGE TEST DATA

Well	Static (M)	72 hr Reading (M)	Drawdown (M)	
TW1	3.47	4.90	1.43	
OW87	3.18	4.10	0.92	
OW85	3.82	4.38	0.56	
OW84	3.94	3.99	0.05	
OW89	3.94	4.72	0.78	

Figure 5 represents the log time versus drawdown plot for the pumping well (TW1) data. An overlay of this plot on the 1987 data (Figure 6) reveals that the hydraulic response of the aquifer was comparable for both continuous discharge tests. The static level recorded in the 1990 test was higher due to seasonal variations in the piezometric surface.

#### 3.4 Groundwater Quality

An assessment of water quality was completed at the end of the 1987 pumping program. The results of the analysis are recorded below. The request for an analysis of the treatability of the water supply necessitated the test well be repumped in May 1990. At that time additional water samples were collected in order to re-test the concentrations of specific geochemical parameters of concern as requested by the Ministry of the Environment.



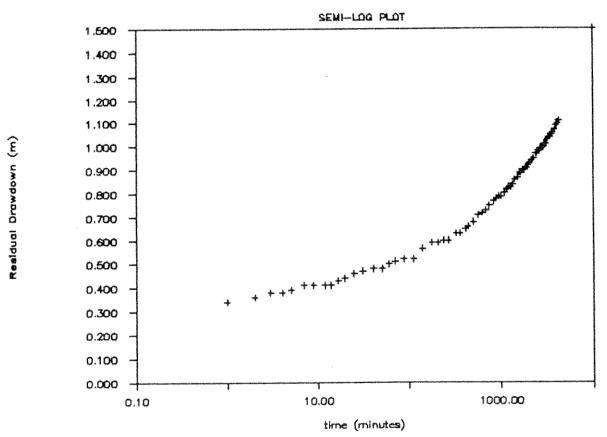
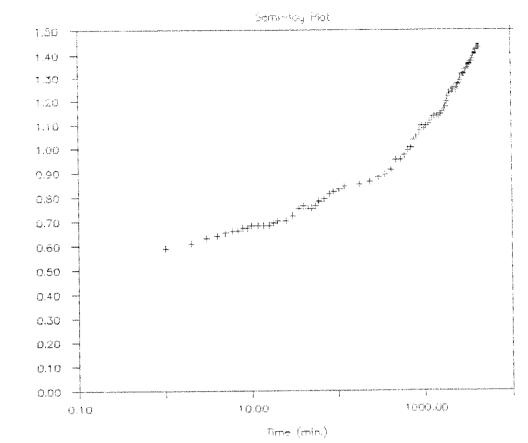


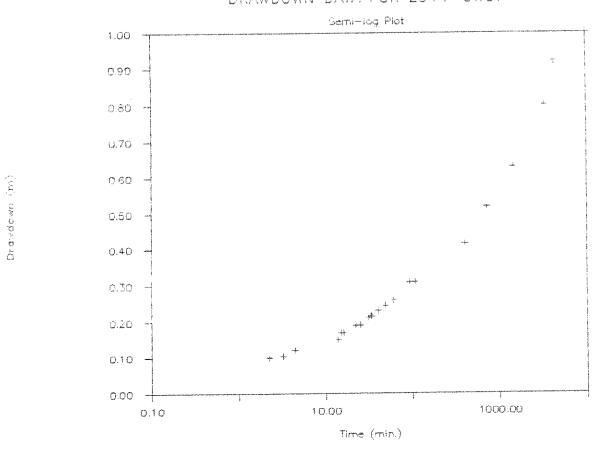
FIGURE 6: Jacob Curve - 1990 Discharge Test

Drawdown (m)

#### DRAWDOWN DATA FOR 2314-TW1



### DRAWDOWN DATA FOR 2314-0W87



#### 3.4.1 Chemical Quality Test Program - 1987

The following water samples were sent to the indicated labs for analysis:

#### Bondar Clegg and Company Ltd., Ottawa

- major ions: 12,24,36,48,60,72 hour and pond water
- trace metals: 12,24,36,48,60,72 hour
- phenols: 24,48,72 hour radionuclides: 72 hour

#### KOPP Clinical Laboratories, Ottawa

- bacteria: 24, 72 hour and pond water

#### Ministry of Health Labs

- bacteria: 24,48,72 hour

#### Mann Testing Laboratories

- volatile and non-volatile organics, pesticides and USEPA 624, 625 priority pollutants: 72 hour

All analytical reports for the analyses performed are contained in Appendix D-1 and are summarized in Table 4 below.

TABLE 4: MAJOR ION AND TRACE METAL GEOCHEMISTRY SUMMARY
All values are in ppm unless otherwise noted.

Parameter	12 hour	24 hour	36 hour	48 hour	60 hour	72 hour
На	7.96	8.09	8.08	8.01	8.03	7.93
Ca	45	45	40	42	42	43
Mg	9	9	8	9	8	8
Na	17	17	17	17	17	17
K	2	2	3	3	2	2
Ba	0.34	0.35	0.32	0.31	0.31	0.28
Hardness	150	150	133	142	138	141
Cl	3	3	3	2	2	2
SO <sub>4</sub>	2	2	3	2	2	2
Alk	160	157	164	163	163	161
F	0.21	0.20	0.20	0.20	0.20	0.20
$PO_4$	0.10	<0.10	0.10	<0.10	0.10	<0.10
As	<0.01	0.01	0.01	0.02	0.02	0.02
В	0.04	0.04	0.05	0.05	0.05	0.06

N-NH <sub>3</sub>	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
$N-NO_3$	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
$N-NO_2$	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
H <sub>2</sub> S <sup>2</sup>		<0.10		<0.10		<0.10
ČN	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
Phen		<0.002		<0.002		<0.002
Total Fe	0.53	0.50	0.50	0.53	0.49	0.48
Mn	0.05	0.05	0.04	0.04	0.04	0.05
Zn	0.01	0.01	<0.01	<0.01	<0.01	<0.01
Cu	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01
Pb	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01
U*	<0.01	<0.01	0.80	0.75	0.70	0.70
Se	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01
Cd	<0.001	<0.001	<0.001	<0.001	<0.001	<0.001
Ag	<0.01	0.01	<0.01	<0.01	<0.01	<0.01
Hg	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Cr	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01
TDS	210	213	207	201	194	184
Cond(umhos)	300	300	320	300	290	290
Colour(UNT)	25	21	16	18	12	15
Turb (NTU)	1.5	0.9	1.2	1.7	1.6	1.6

\*U - values in ppb

Ca Mg Na K Alk Cl  $SO_4$  Tot Fe  $N-NH_3$   $N-NO_2$  TDS Pond Water 12 3 2 1 37 1 9 0.22 <0.10 <0.10 67

#### Bacteria

All bacteria samples tested negative for indicator types with the exception of the sample obtained from the pond which had a total coliform count of 53 col/100 ml.

#### Volatile Organics

The volatile organics scan revealed the presence of the following compounds:

chloromethane dichloromethane trichlorofluoromethane chloroform benzene toluene ethyl benzene P & M xylene O-xylene

Dichloromethane, chloroform and benzene were, however, also detected in the lab water blank. As these constituents are measured at part per billion levels, it is not unusual for samples to erroneously register positive results. All of the above parameters are at concentrations just above minimum detection limits and are well below MOE water quality objectives.

#### Pesticides and Herbicides

All samples tested 'not detected' for pesticide and herbicide analysis.

#### 3.4.2. Chemical Quality Test Program - 1990

Water samples were collected for analysis at 1, 6, 12, 24, 48, and 72 hr intervals. Areco Canada Inc. laboratories of Nepean conducted the analysis for the complete communal water well suite as well as the USEPA 624 suite for volatile organic compounds (VOC). The parameters analyzed for at each of the sampling intervals are listed below.

#### 1 hour sample

hardness ammonia

TKN (Total Kjeldahl nitrogen) nitrate alkalinity

iron (total) chloride nitrite sulphate Hq phenols sulphide gas turbidity fluoride conductivity sodium

calcium TOC uranium potassium magnesium colour

BTXe

Bacti (Tot. col., Faecal col., Faecal strep., background)

#### 6, 12, 24, and 48 hour samples

uranium colour turbidity TOC BTXe  $H_2S$ 

#### 72 hour sample

arsenic barium boron cadmium

chromium cyanide (free)

fluoride lead

mercury nitrate (as N) nitrite (as N) nitrilotriacetic acid (NTA)

```
Pesticides
     aldrin + dieldrin
     carbaryl
     chlordane
     DDT
     diazinon
     endrin
     heptachlor + heptachlor epoxide
     lindane
     methoxychlor
     methyl parathion
     parathion
     toxaphene
     2,4-D
     2,4,5-TP
Radionuclides
     cesium-137
     iodine-131
     radium-226
     strontium-90
     tritium
selenium
                                     methane
silver
                                     odour
turbidity
                                     organic nitrogen
bacti suite
                                     phenols
polychlorinated biphenyls
                                     sulphate
uranium
                                     sulphide
H<sub>2</sub>S gas
                                     taste
chloride
                                     temperature
colour
                                     total dissolved solids
copper
                                     total organic carbon
iron
                                     zinc
manganese
VOC's as per ( USEPA Method 624)
```

Analytical reports from the respective laboratories are contained in Appendix D-2. A summary of the parameters that were of concern to the Ministry of the Environment are shown in Table 5 below. All values are reported in ppm unless otherwise noted.

TABLE 5: 1990 GEOCHEMICAL SUMMARY

Parameters	1 Hr	6 Hr	12 Hr	24 Hr	48 Hr	72 Hr
Fe	0.738	N.A.	N.A.	0.716	0.741	0.008(f) 0.731(u)
Turb. (NTU)	6	6	6	5	5	5 ′
colour (UNT)	25	21	23	25	25	25
$H_2S$ (ppb) 0.	107	0.097	0.070	0.067 0	.008 (np)	0.066
บื	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
TOC	5	6	7	6	6	5
Benzene	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002
Toluene	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002
Ethylbenzene	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002
m,p-Xylene	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002
o-Xylene	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002
EPA 624	N.A.	N.A.	N.A.	ND	N.A.	ND

Quality Control Test Results - 72 Hr. Sample

Novalab, Lachine Quebec EPA 624

Accutest, Nepean Ontario Fe (Tot.) 0.67 (f) phenols < 0.002 Turb. (NTU) <1.0 colour (UNT 32 Ur (ppb) <0.01 TOC 5.7

- (f) filtered sample
- (u) unfiltered sample
- (np) sample not pretreated with preservative
- N.A. not analysed ND not detected

A discrepancy in the filtered Fe (Tot.) results warranted a retest on the sample duplicates. The samples from the 1Hr, 6Hr, 12Hr, 48Hr, and 72Hr sessions that had been filtered and acidified on site were split. One half of the sample was sent to the Areco Canada Inc. laboratory and the remaining half was delivered to the Accutest Ltd. laboratory. The results are as follows;

Laboratory	1HR	6HR	12HR	48HR	72HR
Accutest(ppm) Areco(ppm)					

The Areco Canada Inc. results are within M.O.E. water quality objectives where as the Accutest Laboratories Ltd. data are slightly above the ministry objectives.

#### 4.0 DISCUSSION OF RESULTS

#### 4.1 Water Supply Potential

The glaciofluvial complex situated east of Vars appears to satisfy three of the hydrogeological conditions necessary to meet the water supply demands of the community. These points are listed below and described in subsequent sections.

- The local transmissivity will provide sufficient flow of groundwater to a production well developed at the test well site.
- The water can be extracted by a conventional well design.
- There appears to be a sufficient aquifer extent with associated recharge area to provide for a long term supply.

The aquifer is capable of producing a short term yield to a series of production facilities in excess of the 26.51 l/s (350 IGPM) at which it was tested. The theoretical aquifer yield calculated for the test well is on the order of 68.18 l/s (900 IGPM) over a 20 year design life. The detailed calculation is contained in Appendix F. This estimate is conservative and does not account for seasonal variations in recharge. The aquifer is capable of transmitting this volume of water down its length under an imposed gradient from a production well. The production well would derive recharge from both the north and the south as well as leakage from above and the less permeable bounding deposits.

The 1990 pump test induced a similar hydraulic response in the aquifer as the 1987 test.

#### 4.2 Well Interference

Calculations of well interference are contained in Appendix F. The results, shown in Table 6, indicate that at 1000 metres from a potential production site, an interference of 0.67 metres would be anticipated at a production rate of 11.36 l/s (150 IGPM). This calculation is based on the assumption that both the pumping well and the well that is potentially subject to interference are screened through the same hydrostratigraphic unit. Wells east and west of the esker do not fulfill this condition.

Little significant depression of groundwater piezometric surfaces in the aquifer outside of the immediate area of the well head is forecast. No impact on adjacent water supplies is expected.

TABLE 6: WELL INTERFERENCE RESULTS (IN METRES)

Radius	(M)	150 IGPM	300 IGPM
100		1.03	2.06
500		0.78	1.56
1000		0.67	1.34

Table 7 contains the well drilling and pumping data from wells within 1 km of the Test Well site. Most of the residences and farms in the area draw water from the bedrock aquifer. Overburden wells are often unreported and do not appear in the M.O.E. A survey of wells in the immediate area revealed that a number of shallow dug wells have been developed into the sand unit overlying the clay silt aquitard. This shallow unconfined aquifer would not appear to be hydraulically connected to the water supply aquifer into which the test well is developed. No interference is anticipated. No complaints were received from surrounding property owners during either pump tests.

#### 4.3 Groundwater Quality

The geochemical data listed in Table 5 meets the MOE drinking water objectives for all parameters except for colour, turbidity and iron.

The elevated colour concentrations detected are not uncommon for this type of glaciofluvial deposit, especially those located close to a surface water body in a forested area. This is especially true when the environment is reducing as indicated here. It is believed that colloidal iron is the source of the colour and is associated with the organic components found in the water as indicated by the TOC. The colour turbidity and iron may most likely be removed by treatment. The type of treatment and its cost effectiveness may best be appraised by a complete treatability analysis. An extensive treatability testing program was conducted on the water supply during the Phase III study. The results and conclusions of that study are discussed in a separate report.

To aid in the final well design, the groundwater chemistry results were used in an adapted equilibrium-based speciation model. The model determines the corrosivity or

TABLE 7: MOE WELL DATA

MELL	ני	67		88	7.1		48		1.9		46		45	00	8		160	
DEPTH OF DEPTH OF OVELL	Ş	62		23	48		20		38		57		=	0.5	Ž.		(~)	
OWNER GROLOGIC LOG	FAUBERT A	MALLI CEAL 43 SALES 04 D'AQUST ANDRE	YLLM TPSL 18 BLUK CLAY 50 BLCK GRVL MSND 60 BLCK GRVL 62 BLCK ROCK 67	FAUBERT T GHT CLAY 23 BLOX SHIR AB	THISLE	MSND 15 CLAY 35 GRVL 48 BLCK SHLE 71	ST LOUIS H	CLAY TPSL 20 SHLK 48	GAGNE C	MSND 6 CLATY 38 GRVL 38 SHLK 67	GAVIGES A	CLAY TPSL 19 BLCK SHLE 46		CLAY TPSL 11 BLCK SHLE 45	ST LOUIS P TPSL SAND 15 QSND 40 BLUK CLAY	SAND 60 SAND GRVL 69 ROCK 88	INNES D	YLLW SAND 4 GREY CLAY 23 SAND 72 GRVL SAND 73 SHER 160
WATER	21	2		STD0	90		2		2		2		2	ě	SI IS		8	
TEST	4 1/00	10 1/00			5 1/00		2/00		1/00		3 2/00		2/00	9	10 0/30		1/00	
RATE	~43*	10			ניצו		'n		ı,		دن		ero.	•	oĭ			
LEVEL	18	50			55		თ		32		ರಾ		යා	ć	2		160	
STATIC	44	25		0	20		5		22		9		S	•	2		15	
KIND OF WATER STATIC PUMPED TEST WATER FOUND LEVEL LEVEL RATE	70	99		88	69		40		09	99	40		43	5	9.		155	
CSG KI	4 FR	5 PR		<b>A</b>	3		4 FR		5 FR		4 FR		4 FR		4		6 FR	
크얼	03/22	250 09/71		04/55	01/67		10/62		08/65		29/60		29/60		10/66		250 06/72	
SURFACE	255 03/	250		245 04/	250 01/		250 10/		250 08/		250 09/		720 08/		790 067		250	
ORTHING	475030 5022840	476030 5023680		5021325	5022275		474050 5022390		5022340		474100 5022400		5022400	4 4 4	5022400		475500 5021325	
CON LOT BASTING NORTHING SURFACE DRI BLEV DA	475030	476030		475650	473910		474050		474060		474100		474100		474240		475500	
L01	\$2	25		28	26		97		97		26		26	6	97		28	
CON	-47	₩.		च्या	40		'n		÷		κ.		5	•	r.		ć	
WRLL	*****	~		(C)	-philips		ಸು		9				ဆ	i	<b>්</b>		10	

scaling potential of water pumped from the well. It therefore has implications for the life of the well screen. The results of a model run are shown in Appendix D-1. Calculations indicate that the water is mildly corrosive with a Ryznar Index of 7.7. The model also indicates that the pumped waters are supersaturated with respect to calcium carbonate and some minor encrustation is expected to occur on the well screen.

A review of potential conflicting land uses was undertaken during the course of the investigation. Features such as landfills, sewage lagoons and major transportation routes and other point sources of contaminants were identified. The most significant source of contamination in the area was identified as a small scale farming operation located south of the site. Most of the activities which are associated with water supply contamination are located on the flanks of the esker deposit and therefore isolated by the impermeable clay silt materials. Information to date suggests that, as a result of the hydrogeologically favorable location of the site, no significant conflicts are expected.

Some limited land use control should be exercised by the municipality to protect the well head area. This is generally referred to in the hydrogeological literature as a "well head protection zone". The mechanism by which a municipality institutes such a recommendation may be decided by the municipality in conjunction with their planners. These types of measures are more prevalent in the United States than in Canada and a search for precedent may prove to be valuable.

#### 5.0 PRODUCTION WELL DESIGN AND WELL MAINTENANCE

Information obtained during the drilling, aquifer testing, and geochemical analyses of the groundwater from the test well were used to formulate the final production well design.

The test well was a natural gravel packed well and required 16 hours of developing. A well efficiency of 37.7% at a pumping rate of 26.52 l/s (350 IGPM) was calculated. However, for the production well, a large diameter 250 mm well is preferred. A number of alternatives are available for this well. An artificial gravel packed well (500mm X 250mm) well is preferred in areas where the formation is interbedded. Such a design incorporates a rounded silica gravel pack, sized to the formation, between the 500 mm hole and the 250 mm stainless steel screen. Such a design would be capable of producing in excess of 26.52 l/s (350 IGPM) at a high efficiency. The proposed well design is included in Figure 7.

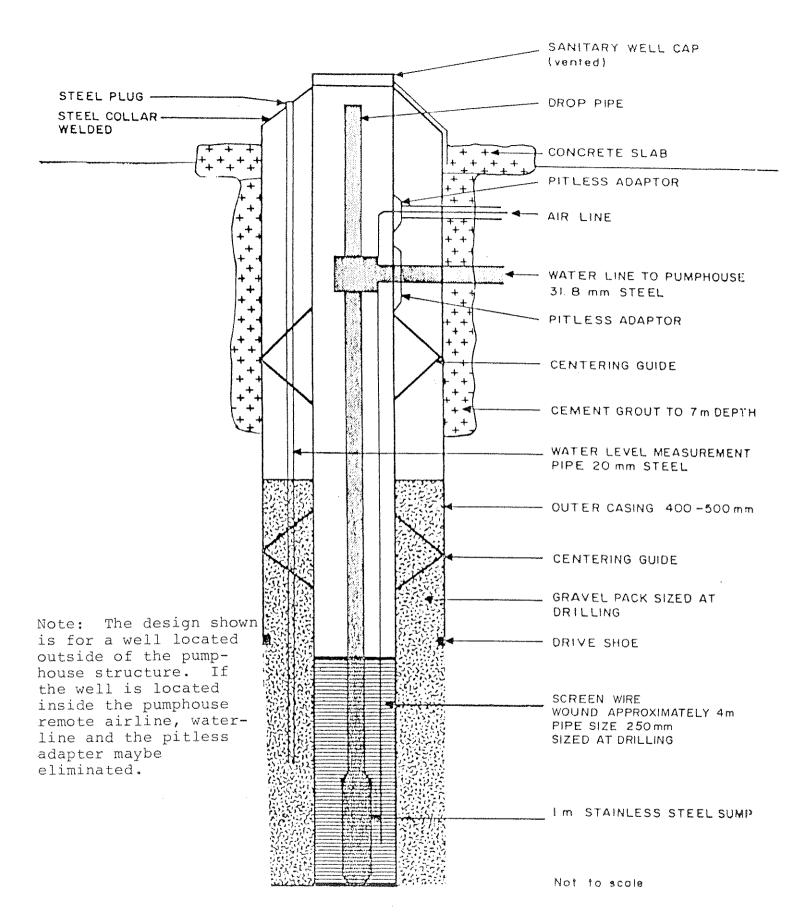


FIGURE 7
PROPOSED WELL DESIGN

It is probable that the installation of a naturally developed well screen is technically feasible at this location. This type of design is less expensive, tends to be more easily developed and if properly designed may be expected to perform as efficiently over the long term as a gravel packed well. Details of the completion are similar to the gravel pack well with the exception of the elimination of the gravel pack and the requirement for different screen design criteria and much more rigorous aquifer material textural and grain size testing. A multi slot size screen design is often the result. MOE policy may restrict the use of this type of well design in a Southern Ontario application.

Regardless of the well design chosen, the final production well may be incorporated into a pump house with a shaft line turbine pump and surface motor or, alternatively, it can be installed outside the pump house and treatment facility if submersible pumping equipment is used. The standby well may be also completed as a stand alone facility if completed with an electrical submersible pump, pitless adapter and above ground vented well head. Baker manufactures such a protective well cap. Minor modification to the existing test well will bring it up to standard.

The final design of the well screen is dependant on the hydrogeological conditions at the production site. This information is only determined at the time of drilling.

The water quality results indicate that in-well chlorination and treatment may be necessary. Precipitates will, with time, accumulate and reduce the overall performance and efficiency of the well. The maintenance program recommended for the production well should most likely include periodic acidification, followed by chlorination to remove precipitates. Maintenance should be undertaken by a qualified well driller/pump installer.

The maintenance schedule should be based on records of well efficiency and specific yield. The latter two factors will be calculated from weekly record of drawdown in the production well and proximal piezometers obtained by the pumping station maintenance staff or an automated system. The measurement water levels should ideally be conducted at the same time and the same day of every week, in order that demand side induced fluctuations in the system may be minimized. Data collected will also be useful in the appraisal of system expansion potential.

Care should be taken that the proper chlorine and acid concentrations are maintained during the cleaning process. Hackett and Lehr (1985) have suggested a free chlorine concentration of between 300 and 500 mg/l over an 18 hour contact time

was effective at killing iron bacteria. A 28% hydrochloric acid is also recommended. Hackett and Lehr (1985) also recommend that the chlorinated water be forced out into the aquifer to ensure proper cleaning of the formation around the well. A surge block will effectively force the water out and also help to physically break up the precipitates. Design of a maintenance schedule will be possible at the conclusion of the first year of operation.

The test well should be modified for use as a standby production well. This will include redevelopment, grouting of the casing and connection and minor well head modifications. The well may or may not be located inside a pump house depending on the final design.

#### 6.0 CONCLUSIONS

The following conclusions have been derived from the work conducted in this study.

- 1. A sand and gravel glaciofluvial complex is present 3 km south east of the village of Vars. A test well was completed approximately 700 metres south of the Devine Road in this complex.
- 2. The Aquifer consists of a narrow band of glacio-fluvial sands and gravels that have been identified in Sarsfield and Leonard to the north and have been traced to Hwy 417 to the south. The Esker is believed to extend further south into Russell Township. A course sand and gravel core runs the length of the deposit and varies in thickness especially north of the site near the Henn pit. The deposit is very relatively thick in the vicinity of the test well. The core of the esker is flanked by a less permeable sand deposit and then by a clay silt unit which, in the vicinity of the test well, confines the aquifer.
- 3. The aquifer has a demonstrated ability to produce in excess of the 26.51 l/s (350 IGPM) design yield required. Phase 2 testing was conducted at a discharge of 26.51 l/s. Theoretical yields were calculated in excess of 68.175 l/s (900 IGPM). At this time a safe perennial yield of 26.51 l/s (350 IGPM) is projected.

- Depression of the water table or piezometric surface occurs 4. at the site of any major groundwater withdrawal scheme. In the case of the Vars well site, the interference effects will be limited due to the fact that few wells are located close to the site. Water table depression due to pumping will most likely be unmeasureable beyond a radius of 500 metres at the projected the projected early system discharge rate of 11.36 l/s. The impact of increased discharge rates is not anticipated to be significant over the long term, for a discharge of up to 26.51 l/s (350 IGPM). Discharges over and above these levels must be investigated further. if any interference on neighbouring farm and domestic water supplies is expected. If such interference does occur it may be easily remedied through either deepening of the well or repair or resetting of the pump.
- or under the village of Vars and is acceptable for public water supply as dictated by the MOE health related criteria (MOE Water Quality Objectives (MOE, 1984). Turbidity in the test well (if used as a standby pumping facility) will improve with additional development and pumping. Turbidity in the production facility is also expected to be below the objective. Constituents in excess of MOE water quality objects are aesthetic in nature and are easily treated either at source or at the end user. These constituents include colour and TOC. The former may be improved through methods discussed in the treatability report found under a separate cover.
- 6. There does not appear to be any potential groundwater contamination sources in the immediate vicinity of the proposed production site. This status should be monitored and possibly some form of land use control be investigated by the municipality. Any spills or potential conflicts should be reported immediately. Access to the well site should be controlled. A provincial system for the immediate reporting of spills already exists, and should serve as an early warning system for the production site.

#### 7.0 RECOMMENDATIONS

The following recommendations have been formulated based on the results of the study.

- 1. The aquifer should be used to meet the long term water supply needs for the village of Vars, with a potentially wider service area at some time in the future. Expansion of the water supply requirements placed on the aquifer, beyond those stated, should be accompanied with appropriate investigations and testing prior to detailed planning. Data collected during the early operation of the wells may be used to this end.
- 2. A 500 x 250 mm artificial gravel pack production well or 250 mm naturally developed well should be installed close to the test well. A separation distance of 10 metres would be sufficient. The well could produce the required 26.51 l/s (350 IGPM). Short term flows that exceed the 26.51 l/s are expected from this arrangement if accommodated by the appropriate pumping equipment.
- 3. A predevelopment survey of all wells within a one kilometre radius of the production site should be undertaken. In the event of a perceived groundwater interference problem at a later time, the well in question should be examined thoroughly and a short report of the condition of the well should be compared to the initial survey. Rural based water supplies in other municipalities have been subjected to substantial criticism, and their ultimate potential reduced due to public opposition and perceived conflicts. The cost of repairing and even replacing allegedly affected water supplies is small in comparison to operating in an adversarial atmosphere.
- 4. A treatability study under separate cover (WESA, 1990) should be referenced regarding the feasibility and costs associated with treatment of the water supply.

Respectfully submitted,

Tami J. Sugarman B.Sc. Hydrogeologist

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Roger M. Woeller, M.Sc. Hydrogeologist

## APPENDIX A Geological Logs

FIGURE		RECORD OF TEST HOLE		DESIGNATION VW7O		MPLE7	TE	
PROJE		VARS WATER SUPPLY		LING METHODS HOLLO		AUGER (	ME 55 DF	ULL_
PROJE	CT NO	1293	DRIL	RVISOR <u>TAMI SUGAT</u> LING CONTRACTOR A	RMAN MARATHO	N DRIL	LING CO.	LTD.
DEPTH METRES	ELEVATION	STRATICRABLY & LIVEROSTRATICRABLY					AMPLIN	
METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY LOG INSTRUMENTATION				TYPE	INTERVAL	N VALUE
						GRAB		
- 0		•						
	ŧ ;	TOPSOIL; sandy silt loam		NOT INSTRUMENTED	<u></u>			
1.2_ -2	t <sup>v</sup>	SAND; fine grained with minor silt matrix (~ 15%)	т					
_								
-4		SILT; grey slurry, minor sand content			•			
		ger, cuess,, manus sums concent		·			r -	
-6			ШШ					
-8				•				
9.1	<u> </u>	SILT; silt slurry with clay matrix	ШШ	·				
-10		Sitt Sidily with Clay matrix						
-		·	聞					
-12 12.2	<u> </u>	CLAY; silty clurry with lenses of					ļ	
		sand			٠			
_14 13.7 <sup></sup>	╅ -	SILT; silt slurry with clay					ļ	
15.2 -	<u> </u>							
-16		End of hole @ 15.24 m (50 ft.) Water encountered at 1.2 m (4 ft.)	-	-			<b>-</b>	
		nater encountered at 1.2 is (4 it.)						
-18			-				<u> </u>	
-20			<b>-</b>			1	<b>-</b>	1 1
		,						
-22			-				<b>-</b>	1 1
-24			-				<b>-</b>	1
-26			-	1			<b>†</b> •	1
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FIGURE		RECORD OF TEST HOLE		DESIGNATION VW 72	COMPLETION DATE 5-6-87					
PROJEC	CT.	VARS WATER SUPPLY	DRII	LING METHODS HOLLO	WSTEM	AUGER (	ME 55 DI			
	T NO		SUPE	ERVISOR <u>TAMI SUGA</u> F	IMAN					
			DRIL	LING CONTRACTOR _N	IARATHO					
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATIO	ON	S	AMPLIN	G		
::L11:L3	ME I NEW					TYPE	INTERVAL	N VALUE		
					***************************************					
						GRAB				
-0 ——	- p	TOPSOIL; sandy laom		Piezometer placed at						
0.76 -	- 1	SILT; sandy content		23.2 m (76 ft.).						
-2 2.1 -		SAND; silty medium grained sand and		Piezometer tip is O. of slotted pipe	.45 m		L -			
3.0 -		granular sized gravel						٠.		
_4		•	00		•					
		SAND AND GRAVEL; fine to medium grained sand with pebble, cobble granule,	~ O -	,			t -			
		gravel occasional boulder	000							
-6		silt matrix (percentage unknown)	~ o . c				<b>-</b>			
			000							
-8			~ O O .				L.			
=		•	000					·		
-10			000			-				
-10			0 0			1	<b>†</b>	1 1		
		•	000							
-12			00				-			
12.8		GRAVEL AND SAND; granules and small	000.0		•					
-14		pebble gravel with a sand matrix	0 6 G			1	L.			
		- silt content	0.00							
40		- intermittent cobbles	3.00				1			
-18	:		0000				r -	1		
			0°358							
-18			8 a Q			1	-	1		
		·	80000	·						
-20			68.5				L.			
			0:00				[·			
			0.00							
- <b>22</b> 22.2 —		TILL; rock fragments and pebble gravel, clayey till					<b>-</b>	1 1		
		,, -,	203.54							
23.8		Bedrock refusal at 23.77 m (78 ft.)	F -				ļ	4		
		Water encountered at 0.76 m (2.5 ft.)								
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FIGURE RECORD OF TEST HO		RECORD OF TEST HOLE	DESIGNATION		COMPLETION DATE			
		THE ONLY OF THE PROPERTY OF TH		VW 75		5-14-87		
PROJE		VARS WATER SUPPLY	DRILLING METHODS HOLLOWSTEM AUGER CME 55 DRILL					
PROJE	CT NO	1293		ERVISOR <u>tami sugaf</u> LING CONTRACTOR N		N DRIL	LING CO.	LTD.
DEPTH	ELEVATION	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATION		SAMPLING		
DEPTH METRES	ELEVATION METRES					TYPE	INTERVAL	N VALUE
						GRAB		
-0	<u> </u>							
		SAND; fine grained, silt (10-15%) rusty oxidized colour		1 1/4" PVC, sletted s	screen,			
-2 1.5	<del> </del>	SAND; fine grained, silty (10-15%)	<b></b> _	placted at 23.57 m be the surface	:10W		L.	]
				(77.3 ft.)			,	
-4			PROTEIN					
4.6	<u> </u>	SAND; fine grained; clay and silt matrix	нин				Γ '	
5.3	╄ -	SILT AND CLAY; slurry with minor sand content						
6.1	┼ -	SILT AND CLAY; sandy, very fine grained					r -	1.
7.6			雕					
_a 7.6 —	Ţ	SILT AND CLAY; stiffer than above with more	開開				'	1
9.4 -	<u> </u>	silt first stone at 8.8 m (29 ft.)				1		
-10 <sup>9,4</sup>		/	翻				<b> </b>	1
10.7	╁ -	SAND AND SILT CLAY; interbedded sands and silty clays	<b>1</b>					
-12		SAND; fine to medium grained grey quartz	1	1				1
	1	sand; unoxidized, unimodal; significant fine; silty fraction,						
-14		low recovery occasional pebble		1			<b>†</b>	1
-16		·					<b>h</b>	
-18	1.		<b>H</b>				<b>-</b>	-
-20			H:::::	4			-	-
							1	
-2221.6	+ -	SAND; coarser, medium to fine grained, fairly unimodal, medium;	-::::				<b>L</b> .	-
22.8		occasional stone	200					
23.5 _ -2423.8 -	‡ :	GRAVEL AND SAND; medium grained sand and pebble gravel					L	_
		TILL; clayey sandy, rock fragment till silty	/					
-26		Bedrock Refual at 23.8 m (28 ft.)	<u>'</u> L.				L	
		Water encountered at 1.5 m ( 5 ft.)						
-28				-			L	_
-20								•
-30	-							
L		WARRANT TO THE TOTAL THE TOTAL TO THE TOTAL THE TOTAL TO		to the second se				
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STOCK COMPANY		The second secon						
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t		<u> </u>		1			. i	



FIGURE	•	RECORD OF TEST HOLE		DESIGNATION VW 76	CC	MPLE <sup>1</sup> 5-15		ATE	
PROJE	СТ	VARS WATER SUPPLY	DRII	LING METHODS HOLLO	WSTEM	AUGER (	OME 55	DRUL	
	CT NO		SUPI	ERVISOR <u>tami sug<b>a</b>r</u>	MAN				
	T		DRIL	LING CONTRACTOR M	ARATH	<del></del>			
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATIO	)N	S	AMPLI	NG	
HE! I'LLO	METRES					TYPE	INTERV	AL N VALUE	
						GRAB			
1.5 -	▼ ▼	SAND; silty, fine grained, (silt ~5-10%)		NOT INSTRUMENTED					
- z	,	SILT AND CLAY; slurry with minor sand					-	1	
3.0 -	† -	SILT AND CLAY; slurry, grey, very wet							
<b>-4</b>		•					-	-	
- <b>6</b> 6.1	ļ .						_	4	
-8		SILT AND CLAY; more stiff than before, increase in silt content, maybe some sandy content near 11.0 m							·
-10		(36 ft.)							
							r	1	1
11.0 - -12 12.1	T -	SAND; fine to medium grained sand							
12.1-		SAND; fine to medium grained sand; occasional stone						,	
-14	<u> </u>	CAND AND CONTROL					-	1	
15.2 16		SAND AND GRAVEL; medium to coarse grained with small pebbles and granules					-	-	
-18			, , ,				_	-	
-20 <sup>19.8-</sup>	<del>-</del> -		P				l ··		
-20		GRAVEL; granule sized gravel and very coarse grained sand matrix						1	
- <b>22</b> 23.2	<u></u>		2000 8000				-	1	
23.5-		TILL; clayey, stoney, sandy, silty till very hard, stiff	<i>F</i>				-	1	
-26		End of hole at 23.5 m (78 ft.) Water encountered at 1.5 m (t ft.) Bedrock nearby	<u>.</u>				-	-	
-28			ļ			,	-		
-30		·						We comment the second s	
								- Avenue Robert Physical Robert Rober	
<b> </b>	- Advantable addisorder and a second additional additio	,	-	and the second s			_	ARCOCCUMPANIA A	
	<b>Б</b> инфи <b>лична</b>		-				F	постинизменного	A CONTRACTOR OF THE PARTY OF TH
	mat object de la faction de la		Name and the second			Meworini MAZMARIII IOO E GA	-	**************************************	AA TEROGRAPH CHILACON
				Bana Artina de la Caración de la Car		***************************************	***************************************		
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		NATION OF THE PROPERTY OF THE		***************************************			THE PROPERTY OF THE PARTY OF TH		
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FIGURE	RECORD OF TEST HOLE	DESIGNATION COMPLETION VW 77 5-15-87					TE
PROJECT	VARS WATER SUPPLY	DRIL	LING METHODS HOLLO	WSTEM	AUGER C	CME 55 DR	ILL
PROJECT NO.		SUPI	ERVISOR <u>tami suga</u> f	RMAN			
		DRIL	LING CONTRACTOR	MARATHO			
DEPTH ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATIO	ON		AMPLING	
		1			TYPE	INTERVAL	N VALUE
					GRAB		
-0	SAND; fine grained sand with ~5% silt		NOT INSTRUMENTED				
1.98	SAND AND CLAY; silty sand and clay mixture (clay is red and green colour).					-	
4.9	SAND; silty (20-30%) very fine grained sand			:			
9.1	SAND; silty (5%) fine grained sand and occasional stone					-	
-10	SAND AND GRAVEL; interbedded sand and large pebble, cobble gravel layers	000				-	-
-12 -14				٠			
-16		000					
-18 <sub>17.9</sub>	GRAVEL; first boulder at 17.9 m (59 ft.) boulder gravel and granules	00000					•
	<b>'</b>	B.0%					
-22 21.9	Till Boulder Till, unable to pass through Clay - very stiff and hard					-	
-24	End of hole at 21.9 m (72 ft.) Water encountered at ~3.0 m (~10 ft.) Bedrock nearby	<u> -                                    </u>				_	
-26		-					
-30				,		-	-
					ANIBVER CANCELLE OF THE	and	Property Commence
- In the second		The second secon					
weareness, seement, s		and sometimes of the sound of t			WANTED A CONTRACTOR OF THE STATE OF THE STAT		**************************************
		William Control of the Control of th			ORTHONOR SANCTON CONTRACTOR OF STREET	Manuscoccoccimination of the Control	gripment Residence Autorithmy Antonia Properties (1900)
		oes konschold ann	A3 14 14 16 16 16 16 16 16 16 16 16 16 16 16 16			Account to make the state of th	Seattle March State Control



FIGURE RECORD OF TEST HOLE				DESIGNATION VW 78	COMPLETION DATE				
PROJE		VARS WATER SUPPLY		LING METHODS HOLLOW		AUGER (	CME 55 DR	ILL_	
PROJE	CT NO	1293	SUPI	ERVISOR <u>tami</u> sugarin LING CONTRACTOR MA	MAN NATHO	N DDII	LING CO	LTD	
DEDTU							AMPLING		
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATIO	N		INTERVAL		
						GRAB			
1.2	<u> </u>	SAND; fine grained golden brown; 5% silt		NOT INSTRUMENTED					
- 2		SAND AND GRAVEL; coarse grained sand with granules and pebbles occasional large stone	,					13 g	
4 8	 		0.0	,	•				
6.1		GRAVEL; granule and pebble gravel in fine grained sand; minor silt, occasional large cobble						A All control or manager up young managers (see	
-10 -12									
-14		Control of the Contro							
-16							_		
-18									
- <b>20</b> 		Boulders at bottom	0000				-		
-22 -24		Till; very stiff clay and sandy till  End of hole at 21.6 m (71 ft.)  Water encountered at ~6.1 m (20 ft.)  moist above this point  Bedrock nearby						*	
-26 : -28		·				,	-		
-30	AND THE PROPERTY OF THE PROPER					Respanse	-		
	Samuel Sa		-			One of the state o	The second state of the se	The second secon	
The second secon	demonstrative of the second of		The state of the s			THE PARTY OF THE P	MACCOURTES PERFER LANGUE PARTY.	Antonia de la factoria del la factoria de la factoria del la factoria de la factoria dela factoria de la factoria de la factor	
The state of the s	·					descriptions of the state of th	The second control of	NA RECEPTOR AND A ACCOUNT OF THE PROPERTY OF T	

FIGURE		RECORD OF TEST HOLE	DESIGNATION COMPLETION DA  VW 79 5-19-87					E
PROJEC	 CT	VARS WATER SUPPLY	DRILI	LING METHODS HOLLO	WSTEM /	AUGER C	ME 55 DRI	
	T NO.		SUPE	RVISOR TAMI SUGAR	MAN			
		,	DRILL	LING CONTRACTOR N	MARATHO		<u>LING CO.</u> AMPLING	
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATIO	ИС			
						TYPE	INTERVAL	VALUE
						GRAB		ŀ
-0								
0.6-		SAND: fine grained, silty (~5% silt)		1 1/4" PVC SCH 40				
<del>-</del> 2		SAND; clayey, fine grained sand and		slotted screen. Pic placted at 22.16 m	ezometer			
-	Z.	silt matrix		(71.7 ft.)	:		1	
3.0 -		CLAY; Champlain Sea clay, red and green minor sand content	HITH					
- 4		SILT AND CLAY; slurry; minor sand content		·			F 1	
•		at top of hed (3.0 m). Smooth clay & silt near 8.8 m.						
-6							<b>-</b>	
•								Ì
-8							<b>-</b> -	
8.8 —	<del>-</del>	SAND; very fine to fine grained~sand	HHHH					
10		with silty content (silt ~15%) - stone at 19.2 m (63 ft.)					<b>-</b>	
		- Stone at 19.2 m (63 ft.)						
-12		·.					<b> </b> -	
			1::::::::::::::::::::::::::::::::::::::					
-14			12					
-16								
<b>⊢18</b>								
-20								
22		sand and boulders						
- <b>22</b> 22.5 _	╀ -	TILL; sandy, very stiff clay and boulder		<b>T</b>				
23.6 <b>-</b>	<b>∔</b> -	till,						
F <sup>2</sup>		Bedrock refusal at 23.6 m (77 ft.)	f -					
	ļ	Water encountered at 2.4 - 2.7 m (8-9 ft.)	l					
-26			T -	•				
- 28			<b>-</b>	-			<b>-</b>	
-30			<b>-</b>				-	·
	***							
<b>l</b>			<b>-</b>	-			<b>-</b>	
				***				
F			h .			****	<b>-</b>	
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FIGURE		RECORD OF TEST HOLE		DESIGNATION VW 80	CO	MPLE7 5-19-8		DATE	
		VARS WATER SUPPLY		LING METHODS HOLLO		AUGER (	ME 55	DRIL	
PROJEC	CT NO	1293		RVISOR <u>TAMI SUGAR</u> LING CONTRACTOR N		N DRIL	LING (	CO. L	TD.
DEPTH	FLEVATION	CTDATIODADUN O INCOCATRATIODADUN					AMPL		
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATION	JIV	TYPE	INTERV	AL N	VALUE
						GRAB			
o	L _								l
0.6		ÖRGANIC SOIL		1 1/4" PVC SCM 40					
1.5		SAND; silty fine grained, orange oxidation; 10% silt	erara:	slotted pipe   Piczometer emplaced a	a t				
•		CLAY; silty, with minor content of fine grained sand		14.5 m (47.7 ft.)			Γ	1	
		grained sand							1
•				·		ļ	<u> </u>	1	
		·							1
6.1	_ Δ	CLAY AND CLUT, clump, com					-	1	
		CLAY AND SILT; slurry, grey	HH						
·8			HH				-	4	Ì
			HH						
-10			HH				-	4	
		increase in sand content near							
11.3 — 12.1 —		SAND AND GRAVEL; fine grained to medium	00				<b> </b>	4	
****		grained sand and granule, pebble gravel	00						
13.7 -	-	SAND; loose sand with minor gravel content	منم				L	_	į
		SAND; interbedded fine grained and fine	1	F					1
15.2 <del>-</del>	╂ -	to medium grained sand	100						1
15.5	<b>↓</b> -	SAND AND GRAVEL; interbedded fine to medium grained sand and pebble granule	0 0				Γ		
		gravel; main seam of gravel at							
-18		15.5 m (51 ft.)	<u>'</u>  -	1		1	<b> </b>	1	
-20		End of hole at 15.5 m (51 ft.) Water encountered within clay and silt							
		layer however good supply is at 11.3 m (37 ft.)							
-22			-	1			-		
								ļ	
-24			<b> </b> .	_			L	4	
-26			L.	<u> </u>					
								1	• .
								- 1	
- 28							ľ	1	•
						· `			
-30			F .				F	-	
								}	1
-			<b> </b> -	-		ļ	F	4	
								Qualitative (Control	
<b>-</b> .			<b> -</b>				L	4	
			Name of the Control o					The state of the s	
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FIGURE		RECORD OF TEST HOLE	- Officer management	DESIGNATION VW 81	co	MPLET	ION DA	TE
PROJE	СТ	VARS WATER SUPPLY	DBII	LING METHODS HOLLO	WSTEM			
	CT NO.		SUPE	ERVISOR TAMI SUGAR	MAN			
			DRIL	LING CONTRACTOR N	ARATHO			
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATION	NC	S	AMPLIN	G
	INC FILE					TYPE	INTERVAL	N VALUE
					***************************************			
						GRAB		
-0 $0.1-$	‡ =	TORCOLL				1		
		TOPSOIL; sandy organic material CLAY; sand, oxidized		NOT INSTRUMENTED		•		
- <b>2</b> 1.5	T -	CLAY; wet, Champlain Sca, red and green		,				
				·				
- 4		*						
4.9	L Z			·		1		
A		SAND; very fine to fine grained; minor silt content ~5%						
•		minor sixt content 5%					r -	
7.3-	+ -	SAND AND SILT; very fine grained sand and	hiiii					
-8		silt slurry	HIIII					
9.1-	<del>-</del>	SAND; very silty (~20%) fine to medium	hiiiiii	,				1 1
-10		grained sand	-			1		
-12								
	1	·						
-14						1		
-14				**************************************			-	
-18			-					1
17.1	+ -	GRAVEL; stone at 12.1 m (56 ft.); fine	00.0.5					
-18		to coarse grained sand and	2003				-	.]
19.2 -	<u> </u>	occasional pebble	6000					
-20		GRAVEL AND SAND; very coarse grained sand and granules; few pebbles and	8 ° C				L.	]
		cobbles						
⊢ <b>22</b> 21.9 -		, , , , , , , , , , , , , , , , , , ,	000					
22.5 -	<u> </u>	IILL; clayey, silty, rock fragment, stiff till	200			Ì		1
			1					
-24		Bedrock refusal at 22.5 m (74 ft.) Water encountered at 4.9 m (16.1 ft.)	<b>-</b>	-			<b>-</b>	-
		aroz encountered at 4.5 m (10.1 10.)				1		
-26							ļ	4 1
		·						
- 28							L	]
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20	-		ATTENNEY AT A TO SEE					
-30			<b>-</b>			İ	r	
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FIGURE		RECORD O	F TEST HOLE		DESIGNATION VW 82	co	MPLE7	ION DA	TE
PROJE	СТ	VARS WATER SUPPLY		DRIL	LING METHODS HOLLO	WSTEM /	AUGER C	ME 55 D	RILL
PROJE(	CT NO	1293		SUPE	RVISOR TAMI SUGAR	RMAN			
				DRIL	LING CONTRACTOR N	MARATHO			
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY &	HYDROSTRATIGRAPHY	LOG	INSTRUMENTATION	NC		AMPLIN	
							TYPE	INTERVAL	N VALUE
							GRAB		
•							0,010		
0.15	F =	TOPSOIL: organic m	aterial and fine sand			<del></del>			
		<u> </u>	Sea clay; red and	<b>'===</b>	NOT INSTRUMENTED				
- 2			ooth, boulder at 3.6 m					<del></del> .	-
		(12 ft.)							
-4								<u> </u>	_
5.2 —									1 1
-6		SAND; fine to mo drilling	edium grained; smooth					L	
6.7 -	_			0					
-8		SAND AND GRAVEL; sma (22 ft.) s	all boulder at 6.7 m medium to coarse	0 0					
~		grained sa	and interhedded with	0.0				<u> </u>	1
		layers of gravel	granule and pobble	0 6					
-10		- occasion	nal cobble layer around					F	-
		16.7 m (55	5 ft.)	° . O					
-12				000				<b> </b> -	4 1
				p 0 0					
-14				°°°°				<u>_</u>	
				000			1		
-16				000					
16.8	_			$\Gamma$ $\circ$ .				r	1
		GRAVEL; boulder at	: 16.8 m (55 ft); also coarse grained sand	0,000					
-18			e and pebble gravel;	40°				<u> </u>	1 l
		granules		000				and the same of th	
-20 19.8 T	† -	TILL; boulder, c	lay till, some silt and	1000				-	4
21.3 -	<u> </u>	rock fragm	ents	FOR 2					
-22		Bedrock refusal at 2		1 -	Name of the state			-	4
		Water encoutered at	5.2 m (17 ft.)						
-24				L					
								F	
				1				Ì	
-26				† ·				T	1
- 28				-	1			<b>-</b>	-
			,				-		
-30							Ì	-	-
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FIGURE RECORD OF TEST HOLE		DESIGNATION COMPLETION DAT  VW 83  5-20-87					ATE			
PROJEC		VARS WATER SUPPLY		LING METHODS <u>HOLLO</u> ERVISOR <u>TAMI SUGA</u> F		AUGER (	CME 55 C	RILL		
PROJEC	CT NO	1293		LING CONTRACTOR N				***************************************		
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATION	ИС	S	AMPLI	1G		
ar i uco	METHES					TYPE	INTERVA	L N VALUE		
					•	GRAB				
_										
0.15==	= =	TOPSOIL; sand and organic material	E. 2002 Sec. 2005	NOT INSTRUMENTED	·····					
	,	SAND; fine grained, silty, clayey sand				Ì				
. 2		CLAY; red and green Champlain Sea					<b>-</b>	1		
		l cray								
. 4	1			4.			<b> </b>	1		
				,						
-6							-	1		
-8							<b>F</b>	1		
9.1 -	- 2		FIET STATES							
-10		SILT AND CLAY; layers of silt and clay with a minor sand content,	開井				r	1		
V.		Very wet slurry Sandy layer at 12.2-12.8 m	囲	,						
-12		Sandy layer at 12.2-12.0 m					F	-		
-14							-	-		
14.9 -	<del> </del>	SAND; fine grained, silty, grey,								
-16		quartzic sand	7:::::::	-			F	-		
-18		· 		,			-	4		
	İ									
- <b>20</b> 19.8 -	<u> </u>	TILL; clay, stiff, bedrock	3-202			1	-	4		
		fragment, sandy tili		VI						
-22		Bedrock refusal at 20.1 m (66 ft.) Water encountered at 9.1 m (30 ft.)	<b>-</b>				-	-		
		,								
-24			<u> </u>				<u>_</u>	-		
-26			ļ	,			_	4		
-28			L .				-			
							ALCONOMIC NAME OF THE PARTY OF	Ì		
-30			<b>.</b> .							
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	A-GREENWAY.			SON THE PROPERTY OF THE PROPER			No. 1 constant	Bengunoswork		
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	and the second second		f '			American (American)	action community of			
	merestilliseddobb.			**************************************		dramedition	irodesservite	MANAGEMENT		
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RECORD OF TEST HOLE				DESIGNATION VW 84	СО	COMPLETION DATE				
PROJE(	CT	VARS WATER SUPPLY	SUPE	LING METHODS <u>HOLLO</u> ERVISOR <u>TAMI</u> SUGAR	MAN					
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	DRIL LOG	LING CONTRACTOR M INSTRUMENTATION		<del>y</del>	LING CO. AMPLING	***************************************		
METRES	METRES	STRATIGRAFHT & HIDROSTRATIGRAFHT	LUG	INSTRUMENTATIO	/IN	TYPE	INTERVAL	N VALUE		
·o						GRAB				
-2		'SAND; fine grained, silt matrix		Piezometer placted 20.5 m (~67 ft.); 1 1/4" PVC, slotte				PETER SERVICE		
3.65		SILT; grey slurry with clay matrix								
-8 9 . 1‴ — -10		CLAY; soft Champlain Sea clay, red and green								
13.0		GRAVEL; granuler and odd pebble	\$0000 \$0000 \$0000							
15.2 16.718		SAND AND GRAVEL; fine to medium grained grey sand and occasional cobble, pebble SAND; fine to medium grained, grey silty sand Boulder at 19.5 m	9 0 o	THE CONTRACTOR OF THE CONTRACT						
23.5 — -2 <sup>4</sup> 23.8 — -26		TILL; sandy, clayey, hard till  Refusal; boulder or bedrock at 23.8 m (78 ft.) Water encountered at ~3.35 m (11 ft.)	STEN			Safatinistica de la casa de la ca				
-28	The state of the s									
-	enorm conficult discussions described and the conficulty of the co			The second secon		A THE STATE OF THE	THE STATE OF THE S			
	A contract of the contract of					Additional Confession of the Confession of C	The second secon	Accessive the second se		



FIGURE		RECORD OF TEST HOLE		DESIGNATION VW 85	CO	MPLET 8-3-	ION DAT	E
PROJE	CT	VARS WATER SUPPLY	DRIL	LING METHODS HOLLO	WSTEM A	UGER C	ME 55 DRI	
	CT NO.		SUPE	ERVISOR <u>tami sugaf</u>	MAN			
DEOTH			DRIL	LING CONTRACTOR <u>M</u>	MARATHO		<u>LING CO.</u> AMPLING	
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATIO	NC			
						TYPE	INTERVAL	VALUE
-0	_							
		SAND; fine grained, boulder at 2.4 m		Piezometer; 1/1/4" P		GRAB		
<b>2</b>	<u>,</u> ,,	(8 ft.) minor silt content		slotted tip; placed a 23.5 m (77 ft.)	t			
_								
_4								
4,6—							<b> </b>	1
5.5		GRAVEL; coarse grained sand or gravel layer	<b></b>					
- <b>6</b> 6.1 —		SAND; fine grained, silty grey SILT; interbedded silt slurry and	<del>╠</del> ┼┼				<b>-</b> -1	
:		clay layers						
-8								
9.1								
-10		SAND; silty, dirty, fine grained sand	HIII-					1
			HIELE:					1
-12			Hill					]
12.5	_	SAND AND GRAVEL; interbedded, fine to	8.70		÷			
-14		medium grained sand and granule, occasional pebble, cobble, boulde	2000				┡ ┤	-
		gravel						
-16		·	300					
			8000					
<b>–18</b>		,	S S				L	1
			6000	;				
-20			00,00					
- <b>22</b> <sup>21.3</sup>	<u> </u>	SAND; fine to medium grained sand.	0 O a					
22.9 -	<u> </u>	SAND; fine to medium grained sand, silty occasional pebble	0					l
	<u> </u>	TILL; bedrock fragments, dirty sandy	i de la constante de la consta	<b>1</b>				1
- <b>24</b> 23.5 **		hard till	个 -	1			T 1	. [
		Refusal at 23.5 m (77 ft.) Water encountered at ~1.5 m (5 ft.)						
-26			<u> </u>					1
	ŀ							
- 28			<b>!</b>	1		1	<b> </b>	, .
-30			<b>-</b>	1			<b>-</b>	NAVA CALL
		observation of the control of the co	**************************************					
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		**************************************						
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-		- Facility of the Control of the Con	<b>+</b> .	-			<u> </u>	
	endolf red de sea	Tanana and Tanana and					Name of the last o	,
	<u> </u>		Tanana II			1		l



FIGURE	•	RECORD OF TEST HOLE		DESIGNATION VW 86	CO	MPLE7	ION DAT	Έ
PROJE	СТ	VARS WATER SUPPLY	DRIL	LING METHODS HOLLO	WSTEM			
	CT NO		SUPE	ERVISOR <u>tami sugar</u>	MAN			
			DRIL	LING CONTRACTOR M	ARATHO			
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATIO	N		AMPLING	
						TYPE	INTERVAL	1 VALUE
							,	
-0								•
		'SAND; silty, golden brown	a i	1 1/4" PVC, slotted		GRAB		
	\(\sigma\)	onary gorden (nomi		piezometer placed at				
- 2			-	23.3 m (76 ft.)				
3.0	<del>-</del>				-			
-4		SILT; sandy, occasional pebble clayey slurry	$H \mid \cdot \mid +$					
		·						- 1
-6			$H \cap H$					
-8							L	- 1
•								
9.1 <del></del> -10	† -	CLAY						1
-10		CDAT					1	
-12		·				,	┞┤	
-14 13.7	_	SILT AND CLAY	HITT				┡╶┤	
			田田	***************************************				
-16		·	開封				L 1	
16.8	<u> </u>		田田					
-18		SILT AND SAND						Ì
18.3	<u> </u>						1	
••		SAND; silty, fine to medium grained						
-20							F 1	]
-22			F				F -	
		·		Ħ				
-24				<b>.</b>			<u> </u>	
24.4	<del> -</del>	End of hole at 24.4 m (80 ft.)	<u> </u>					
26		Water encountered at 1.5 m (5 ft.)	L .					
		and 18.3 m (60 ft.)						
**								
- 28			_					·
		-						
-30			<b>-</b>				<b>-</b>	
	the state of the s							
<b>-</b>		The second					_	
	·		***************************************	The second secon			***************************************	
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		and in the contraction of the co			-	-	Name of the last o	
<b>-</b>	2	remains a second of the second	L	]		Polymania (Polymania (	manusere	
				Accompany of the Control of the Cont				Action to the second se
		·		elininiment.			C-Level State of the Colonial State of the C	
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	NA CONTRACTOR OF THE CONTRACTO	Transmission of the Control of the C				949938889466		
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FIGURE		RECORD OF TEST HOLE		DESIGNATION VW 87	со	COMPLETION DATE				
PROJEC	T	VARS WATER SUPPLY	DRIL	ING METHODS HOLLO	WSTEM	AUGER CME	55 DR	ILL_		
	T NO		DRIL	RVISOR TAMI SUGAL LING CONTRACTOR I	MARATHO	N DRILLING	3 CO.	LTD.		
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATI	ON	TYPE INT	PLIN( ERVAL			
0			ļ	1						
. 2	Ż	SAND; fine grained, top few layers are oxidized rusty orange, rest is grey		Piezometer 1 1/4", s pipe placed at 23.7 (~78 ft.). Screen i 0.47 m in length.	m	-	-			
· <b>4</b>							-			
- <b>6</b> 5,5	<u> </u>	SILT AND CLAY; silt slurry with layers of clay and clay matrix					-			
-8										
-10										
11.4 ~	† -	SAND AND GRAVEL; granule to pebble gravel and medium grained sany layers interbedded	000	C C				-		
-14			0000							
-16			TO 0					***************************************		
16.8 ·		GRAVEL; granule to pebble; cobble grave; sand matrix	0.000000000000000000000000000000000000	30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.000 30.0000 30.000						
-20				40 a 00			_			
-22			10000000000000000000000000000000000000	04 00 00 00 00 00			-			
-24			200	्त् 4						
24.7 26		TILL; clayey, bedrock fragment, sandy till	FF	7			-	-		
-28		End of hole at 25 m (82 ft.) Water encountered at 1.2 m (4 ft.)	-				<b>-</b>	-		
-30	evverient in the second little		-				-	-		
	manus epistemines de description de la compansión de la c			,			WARRING TO THE TOTAL THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE	- Committee Comm		
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To a company of the c			A STATE OF THE STA	-			A CONTRACTOR OF THE PROPERTY O	1		
	Name of the Control o		nematric relations (November 1997)				NAMES OF THE PROPERTY OF THE P			

FIGURE	-	RECORD OF TEST HOLE				LETION DATE			
			DRILLING METHODS HOLLOWSTEM AUGER CME 55 DRILL						
PROJE		VARS WATER SUPPLY	CHE	RVISOR TAMI SUGAF	MAN				
PROJE	CT NO	1293	DRILLING CONTRACTOR MARATHON DRILLING			LING CO.	LTD.		
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATION	INSTRUMENTATION		AMPLIN INTERVAL		
				,					
0.46	_	ORGANIC PEAT SOIL		Piezometer placed at	22.9 m				
0.40		SAND: very fine to fine grained sand,		(75 ft.), 0.3 m slot	ted				
2	1	light brown to grey	-	1 1/4" screen, PVC			<u> </u>	1 1	
3.0 -		SILT AND CLAY; silt slurry with clay blobs	HH						
4		and matrix	曲韻		۴		<b>†</b> '		
			開動						
-6								1 1	
		A CONTRACTOR OF THE CONTRACTOR							
-8				1			1	1	
		Sandy layer at 9.1 m (30 ft.)	HH						
<b>-10</b> .9.7	+ -	GRAVEL LAYER; large cobbles or boulders, lag	0000				-	-	
10.7-	+ -	SAND; very compact, stiff drilling,	1			1			
-12		granule layer at 11.9-12.2 m (39-40 ft.) medium to coarse	<b>F</b>				-	1	
		grained (39-40 ft.) medium to coarse							
-14				-			ŀ	1	
				Control of the contro					
-1 <b>6</b> <sup>15</sup> . 2 -		GRAVEL AND SAND; coarse to medium grained	200				F	-	
16.7 -		sand and granule and pebble gravel	0				1		
-18		SAND; medium to coarse grained gravel	- L				F	+	
		layer at 20.6 m (67.5 ft.)							
-20							-	-	
-22							-	4	
		,							
						1	-	-	
-24		1							
25.0		BOULDER LAYER	00	<u> </u>			-	4	
-26 25 . 7. 26 . 2		TILL	2.00	6					
		End of hole at 26.2 m (86 ft.)	L				-	1.	
-28		Water encountered at 1.5 m (5 ft.)	Γ					THE STATE OF THE S	
							_	4	
-30	i i		Γ	7					
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+			-						
				B-1-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-		The state of the s	and the second s		
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						The state of the s	000	No.	
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	and the second s		Second Se			Overline market		GO-AMERICAN PARTY.	
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FIGURE		RECORD OF TEST HOLE	DESIGNATION VW 89		COI	COMPLETION DATE		
PROJE		VARS WATER SUPPLY	DRILLING METHODS HOLLOWSTEM AUGER CME 5				ILL	
	CT NO		SUPE	RVISOR TAMI SUGAR	MAN			
			DRIL	LING CONTRACTOR N	OHTARAN		LING CO. AMPLING	
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY & HYDROSTRATIGRAPHY	LOG	INSTRUMENTATION	ИС			
						ITPE	INTERVAL	N VALUE
-0								
	C**	SAND; fine grained sand, oxidized to 1.8 m (6 ft.) orangey, golden		Piezometer placed at m (75 ft.), 1 1/4 "	22.86 PVC			
- 2	_52_	brown, below 1.8 m grey stiff	_	slotted screen (~0.6				
		sand. Between 2.6-3.0 m sand with occasional pebble. From		1				
-4		20-4.6 m increase in silt content						
4.6	_	SILT AND CLAY; sandy layer at 6.1 to 6.7 m						l
-6		(20-22 ft.)						
			掛掛					
-8								
8.7 -	<b>├</b> ▽	BOULDER	0.0.0					
10		GRAVEL AND SAND; interbedded, medium to coarse grained sand and granule,	00				<b>-</b>	
		pebble, and possibly cobble	000					
-12		gravel	0 0 (				-	
			0.0					
-14			000	1			<b>-</b>	
			0.0					
-16			00					
			°0, 0	American de la companya de la compan				
-18			-000				-	
			0.00					
-20			, o O					1 1
			00	4				
-22			600				<b>-</b>	1 1
		·	00	P		-		
-24 23.6-	<u> </u>	TILL; granule and bedrock fragment	200				<b>-</b>	
24.1		shale in clay and sand matrix	4					
-26		End of hole at 24.1 m (79 ft.) Water encountered at 1.5 m (5 ft.)	-				<b>-</b>	
		nater encountered at 1,3 m (5 ft.)						
- 28			F				-	-
						TANK THE PERSON THE PE		
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	and the second			***			<b>W</b>	
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FIGURE		RECORD OF TEST HOLE	DESIGNATION VW 90			COMPLETION DATE			
PROJE	CT	VARS WATER SUPPLY	DRILLING METHODS HOLLOWSTEM AUGER CME 55 I			DRILL			
	CT NO		SUPE	RVISOR TAMI SUGAR	MAN				
			DRILL	<u> ING CONTRACTOR M</u>	ARATHO				
DEPTH METRES	ELEVATION METRES	STRATIGRAPHY 8 HYDROSTRATIGRAPHY	LOG	INSTRUMENTATIO	ON L		AMPLI		
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			<u> </u>			TYPE	INTERVA	AL N VALUE	
0.3 —	<u> </u>	ORGANIC SOIL		Piczometer placed a				1	
	7	SAND; fine grained, silty sand,		22.5 m (73.8 ft.) 1	1/4"				
1.5 -		silt ~20% SILT AND CLAY; silt and clay lump slurry	饵到	PVC pipe with 0.48 slotted screen	m l		<b> -</b>	4	
		with minor sand	脏组	Signed Serecii					
. 4		Sand layer at 7.8-9.1 m -(23.5-30 ft.)	田封		l				
7		(20.0 50 10.)	田田		-		<b>-</b>	٦	
			田田					1	
. 8					ĺ		F	4	
			田田		į				
-8			開題	***************************************			L	-	
			田封					1	
9.1 -10	T -	CLAY							
								7	
•									
12.2-	<del> -</del> -	· · · · · · · · · · · · · · · · · · ·					<b>-</b>	4	
		CLAY AND SAND							
-14			142341				L		
-16 <sup>15.5</sup>	╆ -		100						
~10		SAND AND GRAVEL; medium to coarse grained	000				F	1	
		sand interbodded with granule and pebble gravel layers	000		İ				
-18		(few cobbles near bottm)	69				-	4	
			6.0						
-20			0 0				L		
			000						
			0 0						
- <b>22</b> 22 <b>.</b> 1	<u> </u>	(77.5.1	1.0				<b>†</b>	1	
22.9	+ -		1824-261						
-24		End of hole at 22.9 m (75 ft.) Water encountered at 1.5 m (~5 ft.)	<u> </u>				<b> </b> -	4	
-26			L				L	_	
20			Γ -			1	ſ		
			ı						
- 28			<b>-</b>				r	1 .	
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-30	## ### ### ## ## ## ## ## ## ## ## ## #			_			<b> </b> -	4	
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	TROUBLE STORY		***************************************			Notice designation of the last		EVENERAL VA	
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# APPENDIX B Step Drawdown Test Data

Type of aquifer test:	STEP TEST Well type:	PUMPING
How Q Measured:	ORIFICE WEIR Data type:	PUMPING
How w. l.'s measured:	W.L. TAPE Depth pump:	18.30 m

Rad./dist. from pumping well: 0 m Pump on: 06-10-87 15:00:00

Meas. point for w. l.'s(m): T.O.C. Pump off: 06-10-87 18:00:00

Ground Elevation (masl): Discharge rate: 100,200,300,400

Static Water Level (m): 4.36 513 IGPM

Time	W.L.		Discharge	
from start of test		Drawdown	rate	COMMENTS
(minutes)	) (m)	s (m)	Q (IGPM)	
1.0	0 4.450	0.090	100	
2.0		0.065		
3.0		0.055		
4.(		0.070		
5.0	0 4.430	0.070		
6.0	0 4.435	0.075		
7.0	0 4.420	0.060		
8.0		0.060		
9.0		0.070		
10.0		0.070		
12.0		0.070		
14.0		0.070		
16.0		0.070		
18.0		0.070		
20.0		0.070		
22.0		0.070		
24.0		0.070		
26.0		0.070		
28.0		0.070		
30.0		0.070	200	
31.0		0.150		
32.0		0.150		
33.(		0.170		
34.(		0.165		
35.0 36.0		0.165 0.170		
37.0		0.170		
38.0		0.170		
39.0		0.170		
40.0		0.170		
42.0		0.175		
44.0		0.175		
46.0		0.175		
48.0		0.175		
50.0		0.175		
52.0		0.180		
54.0		0.175		
56.0		0.180		
58.0		0.200		
60.0		0.210		

WELL#: TW 1

Type of aquifer test:	STEP TEST W	ell type:	PUMPING
How Q Measured:	ORIFICE WEIR D	ata type:	PUMPING
How w. l.'s measured:	W.L. TAPE D	epth pump:	18.30 m

Rad./dist. from pumping well: 0 m Pump on: 06-10-87 15:00:00

Meas. point for w. l.'s(m): T.O.C. Pump off: 06-10-87 18:00:00

Ground Elevation (masl): Discharge rate: 100,200,300,400

Static Water Level (m): 4.36 513 IGPM

Time	W.L.	Residual	Discharge	
from start of test	reading	Drawdown	rate	COMMENTS
(minutes)	(m)	s (m)	Q (IGPM)	
		0.045	200	
61.0	4.705	0.345	300	
62.0	4.680	0.320		
63.0	4.720	0.360		
64.0	4.710	0.350 0.350		
65.0 66.0	4.710 4.710	0.350		
67.0	4.710	0.350		
68.0	4.720	0.360		
69.0	4.720	0.360		
70.0	4.730	0.370		
72.0	4.730	0.370		
74.0	4.730	0.370		
76.0	4.730	0.370		
78.0	4.740	0.380		
80.0	4.730	0.370		
82.0	4.735	0.375		
84.0	4.740	0.380		
86.0	4.780	0.420		
88.0	4.745	0.385		
90.0	4.750	0.390		
91.0	4.910	0.550	400	
92.0	4.930	0.570		
93.0	4.940	0.580		
94.0	4.930	0.570		
95.0	4.930	0.570		
96.0	4.950	0.590		
97.0	4.950	0.590		
98.0	4.950	0.590		
99.0	4.950	0.590		
100.0	4.950	0.590		
102.0	4.950	0.590		
104.0	4.960	0.600		
106.0	4.960	0.600		
108.0	4.960	0.600		
110.0	4.965	0.605		
112.0	4.960	0.600		
114.0	4.970	0.610		
116.0	4.965	0.605		
118.0	4.970	0.610		
120.0	4.975	0.615		

JOB#1293

WELL#: TW 1

Type of aquifer test: STEP TEST Well type: PUMPING How Q Measured: ORIFICE WEIR Data type: PUMPING How w. l.'s measured: W.L. TAPE Depth pump: 18.30 m

Rad./dist. from pumping well: 0 m Pump on: 06-10-87 15:00:00 Meas. point for w. l.'s(m): T.O.C. Pump off: 06-10-87 18:00:00 Ground Elevation (masl): Discharge rate: 100,200,300,400

Static Water Level (m): 4.36 513 IGPM

Time	W.L.		Discharge	
from start of test	reading	Drawdown	rate	COMMENTS
(minutes)	(m)	s (m)	Q (IGPM)	
121.0	5.110	0.750	513	
122.0	5.110	0.750		
123.0	5.120	0.760		
124.0	5.120	0.760		
125.0	5.125	0.765		
126.0	5.125	0.765		
127.0	5.125	0.765		
128.0	5.130	0.770		
129.0	5.130	0.770		
130.0	5.130	0.770		
132.0	5.130	0.770		
134.0	5.135	0.775		
136.0	5.140	0.780		
138.0	5.140	0.780	₩,	
140.0	5.140	0.780		
142.0	5.145	0.785		
144.0	5.150	0.790		
146.0	5.155	0.795		
148.0	5.160	0.800		
150.0	5.165	0.805		
155.0	5.165	0.805		
160.0	5.170	0.810		
165.0	5.170	0.810		
170.0	5.175	0.815		
175.0	5.180	0.820		
180.0	5.185	0.825	<	C-PUMP OF

Type of aquifer test:	STEP TEST Well type:	OBSERVATION
How Q Measured:	ORIFICE WEIR Data type:	PUMPING
How w. l.'s measured:	W.L. TAPE Depth pump:	18.30 m

Rad./dist. from pumping well: 3.5 m Pump on: 06-10-87 15:00:00

Meas. point for w. l.'s(m): T.O.C. Pump off: 06-10-87 18:00:00

Ground Elevation (masl): Discharge rate: 100,200,300,400

Static Water Level (m): 3.76 513 IGPM

Time	W.L.		Discharge	
from start of tes (minutes		Drawdown s (m)	rate Q (IGPM)	COMMENTS
4	2 200	0.040	100	
1.		0.040 0.040	100	
5.		0.040		
6.		0.040		
7.		0.040		
8.		0.040		
9.		0.040		
10.	.0 3.800	0.040		
12.		0.070		
14.		0.070		
16.		0.070		
18.		0.040		
20.		0.040		
22.		0.040		
24.		0.040		
26. 28.		0.040 0.040		
30.		0.040	200	
31.		0.060	200	
32.		0.080		
33.		0.080		
34.		0.080		
35.		0.090		
36.		0.090		
37.	.0 3.850	0.090		
38.		0.090		
39.		0.090		
40.		0.090		
42.		0.100		
44.		0.110		
46.		0.110		
48.		0.120		
50.		0.120		
52.		0.120		
54.		0.120		
56.		0.130		
58.		0.130		
60.		0.130	222	
61.		0.130	300	
62.	.0 3.920	0.160		

Type of aguifer test:	STEP TEST Well type:	OBSERVATION
How Q Measured:	ORIFICE WEIR Data type:	PUMPING
How w. l.'s measured:	W.L. TAPE Depth pump:	18.30 m

Rad./dist. from pumping well: 3.5 m Pump on: 06-10-87 15:00:00 Meas. point for w. l.'s(m): T.O.C. Pump off: 06-10-87 18:00:00 Ground Elevation (masl): Discharge rate: 100,200,300,400 Static Water Level (m): 3.76 513 IGPM

÷	Time from start of test	W.L. reading	Drawdown	Discharge rate	COMMENTS
	(minutes)	(m)	s (m)	Q (IGPM)	
	63.0	3.920	0.160		
	64.0	3.920	0.160		
	65.0	3.920	0.160		
	66.0	3.920	0.160		
	67.0	3.920	0.160		
	68.0	3.930	0.170		
	69.0	3.930	0.170		
	70.0	3.930	0.170		
	72.0	3.930	0.170		
	74.0	3.930	0.170		
	76.0	3.940	0.180		
	78.0	3.940	0.180		
	80.0	3.940	0.180		
	82.0	3.940	0.180		
	84.0	3.940	0.180		
	86.0	3.950	0.190		
	88.0	3.950	0.190		
	90.0	3.950	0.190	400	
	91.0 92.0	3.960	0.200	400	
	93.0	3.970 3.980	0.210 0.220		
	94.0	3.980	0.220		
	95.0	3.980	0.220		
	96.0	3.980	0.220		
	97.0	3.980	0.220		
	98.0	3.980	0.220		
	99.0	3.980	0.220		
	100.0	3.990	0.230		
	102.0	3.990	0.230		
	104.0	3.990	0.230		
	106.0	4.005	0.245		
	108.0	4.005	0.245		
	110.0	4.003	0.243		
	112.0	4.003	0.243		
	114.0	4.003	0.243		
	116.0	4.003	0.243		
	118.0	4.003	0.243		
	120.0	4.003	0.243		
	121.0	4.003	0.243	513	
	122.0	4.004	0.244		

AQUIFER TEST DATA

JOB#1293

WELL#: TH87

<-PUMP OFF

Type of aquifer test: STEP TEST Well type: OBSERVATION How Q Measured: ORIFICE WEIR Data type: PUMPING How w. l.'s measured: W.L. TAPE Depth pump: 18.30 m

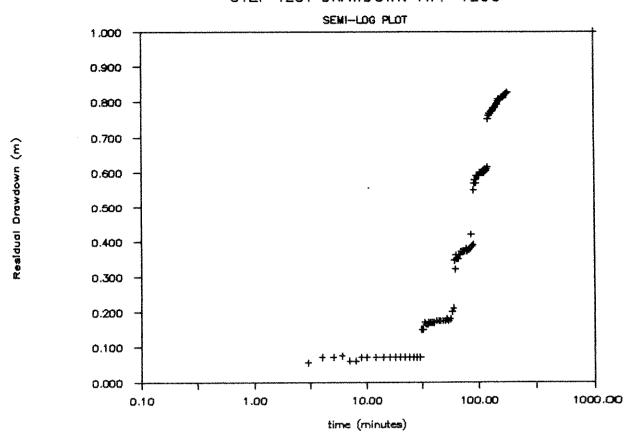
Rad./dist. from pumping well: 3.5 m Pump on: 06-10-87 15:00:00 Meas. point for w. l.'s(m): T.O.C. Pump off: 06-10-87 18:00:00 Discharge rate: 100,200,300,400

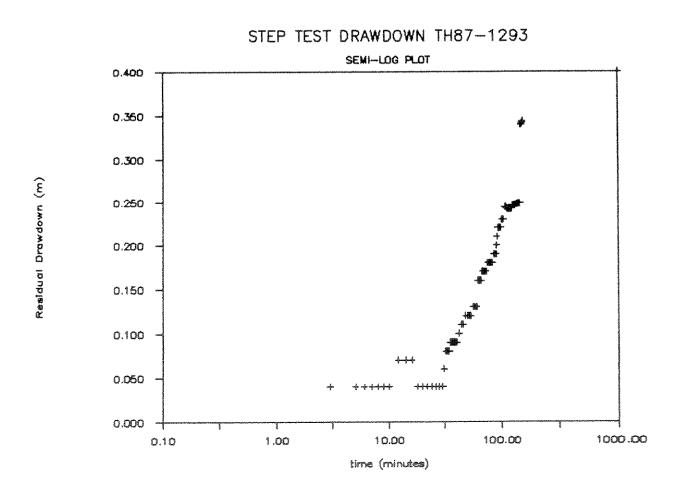
Static Water Level (m): 3.76 513 IGPM

180.0

Time from start of test (minutes)	W.L. reading (m)	Residual Discharge Drawdown rate s (m) Q (IGPM)	COMMENTS
123.0	4.007	0.247	
124.0	4.007	0.247	
125.0	4.007	0.247	
126.0	4.007	0.247	
127.0	4.007	0.247	
128.0	4.007	0.247	
129.0	4.007	0.247	
130.0	4.007	0.247	
132.0	4.008	0.248	
134.0	4.008	0.248	
136.0	4.008	0.248	
138.0	4.009	0.249	
140.0	4.009	0.249	
142.0	4.009		
		0.249	
144.0	4.009	0.249	
146.0	4.100	0.340	
148.0	4.100	0.340	
150.0	4.102	0.342	
152.0	4.104	0.344	

# STEP TEST DRAWDOWN TW1-1293





# APPENDIX ·C

# Aquifer Test Data and Calculations

C-1 1987 Test Program C-2 1990 Test Program

Type of aquifer test:	CONST.DISCHARGE	Well type:	PUMPING
How Q Measured:	ORIFICE WEIR	Data type:	PUMPING
How w. l.'s measured:	_	Depth pump:	18.3 m

Rad./dist. from pumping well: 0 m Pump on: 07-10-87 16:00:00
Meas. point for w. 1.'s(m): T.O.C. Pump off: 10-10-87 16:00:00
Ground Elevation (masl): Discharge rate: 350 IGPM
Static Water Level (m): 4.36 Length of Test: 72 HRS

Time	W.L.	Residual	Discharge	
from start of test	reading	Drawdown	rate	COMMENTS
(minutes)	(m)		Q (IGPM)	
1 0	. 200	0.240	<b>&gt; F O</b>	
1.0	4.700	0.340	350	<-weak H2S
2.0	4.720	0.360 0.380		odoyr
3.0 4.0	4.740	0.380		<-clear
5.0	4.750	0.390		CICAL
7.0	4.770	0.410		
9.0	4.770	0.410		
12.0	4.770	0.410		
14.0	4.770	0.410		
17.0	4.790	0.430		
20.0	4.800	0.440		
25.0	4.820	0.460		
31.0	4.830	0.470		
40.0	4.840	0.480		
50.0	4.840	0.480		
60.0	4.860	0.500		
70.0	4.870	0.510		
88.0	4.880	0.520		
112.5	4.880	0.520		
141.5	4.925	0.565		
180.0	4.950	0.590		
210.0	4.950	0.590		
243.0	4.960	0.600		
273.0	4.960	0.600		
332.0	4.990	0.630		
363.5	4.990	0.630		
420.0	5.010	0.650		
447.0	5.020	0.660		
510.0	5.040	0.680		<-disch.
572.0	5.070	0.710		broke, flow
630.0	5.080	0.720		back towards
693.0	5.090	0.730		well at v.
749.0	5.110	0.750		slow rate
839.0	5.130	0.770		
905.0	5.140	0.780		/ #in=h
960.0	5.150	0.790		<-disch.
1020.0	5.150	0.790		repaired <-still H2S
1110.0	5.165	0.805 0.820		odour
1170.0	5.180	0.830		VUVUL
1227.0	5.190	0.030		

JOB#1293

WELL#: TW 1

Type of aquifer test: CONST.DISCHARGE Well type: PUMPING How Q Measured: ORIFICE WEIR Data type: PUMPING How w. 1.'s measured: W.L. TAPE Depth pump: 18.3 m Rad./dist. from pumping well: 0 m Pump on: 07-10-87 16:00:00 Meas. point for w. 1.'s(m): T.O.C. Pump off: 10-10-87 16:00:00

Ground Elevation (masl): Discharge rate: 350 IGPM Discharge rate: 350 IGP 4.36 Length of Test: 72 HRS Static Water Level (m):

Time	W.L.	Residual	Discharge	
from start of t		Drawdown	rate	COMMENTS
(minut		s (m)	Q (IGPM)	
128	8.0 5.190	0.830		
135		0.840		
141		0.860		
152		0.870		
159		0.890		
165		0.890		
173		0.900		
181		0.900		
187		0.910		
195		0.920		
205		0.930		
214		0.940		
226		0.950		
237		0.970		
243		0.970		
250		0.980		
256		0.980		
262	3.0 5.350	0.990		
268		0.990		
274		0.990		
284	8.0 5.355	0.995		
292	2.0 5.370	1.010		
298		1.010		
310		1.010		
319		1.030		
328		1.040		
340	0.0 5.400	1.040		
352		1.050		
364		1.060		
379		1.070		
394	0.0 5.450	1.090		
409		1.100		
422	7.0 5.470	1.110		

JOB #1293 WELL#: TW 1

Type of aquifer test: CONST. Q Well type: PUMPING How Q Measured: ORIFICE WEIR Data type: RECOVERY Distance from pumping well: 0 Depth pump: 18.3 m Meas. point for w. l.'s: T.O.C. Pump on: 07-10-87 Elevation of Measuring Pt.: Pump off: 10-10-87 RECOVERY

07-10-87 16:00:00 10-10-87 16:00:00

Static Water Level: 4.36 Discharge rate: 350 IGPM

At t' = 0, t =				
Minutes		4320	Water, Level Dat	
1 4321.0 5.180 0.820 2 2161.0 5.120 0.760 3 1441.0 5.110 0.750 4 1081.0 5.110 0.750 5 865.0 5.100 0.740 6 721.0 5.100 0.740 7 618.1 5.100 0.740 8 541.0 5.095 0.735 10 433.0 5.095 0.735 11 430.0 5.095 0.735 12 361.0 5.095 0.735 14 309.6 5.085 0.725 16 271.0 5.080 0.720 18 241.0 5.080 0.720 18 241.0 5.080 0.720 217.0 5.080 0.720 22 197.4 5.075 0.715 22 197.4 5.070 0.710 24 181.0 5.060 0.700 26 167.2 5.060 0.700 28 155.3 5.055 0.695 30 145.0 5.050 0.695 30 145.0 5.050 0.695 31 124.4 5.040 0.680 40 109.0 5.035 0.675 45 97.0 5.035 0.675 45 97.0 5.035 0.675 55 79.5 5.020 0.660 60 73.0 5.050 0.695 80 55.0 5.010 0.685 80 55.0 5.010 0.685 80 55.0 5.010 0.685 80 55.0 5.010 0.685 80 55.0 5.010 0.685 80 55.0 5.010 0.660 178 25.3 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 214 21.2 4.975 0.615 215 0.500 0.5640 407 11.6 4.910 0.550 449 10.6 4.900 0.540 493 9.8 4.890 0.530			•	
2       2161.0       5.120       0.750         4       1081.0       5.110       0.750         4       1081.0       5.110       0.750         5       865.0       5.100       0.740         6       721.0       5.100       0.740         7       618.1       5.100       0.740         8       541.0       5.095       0.735         10       433.0       5.095       0.735         10       433.0       5.090       0.730         12       361.0       5.085       0.725         16       271.0       5.085       0.725         16       271.0       5.080       0.720         20       217.0       5.075       0.715         21       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         50       87.4       5.030       0.675         50       87	minutes	t/t'	w.1. (m)	Drawdown
2       2161.0       5.120       0.750         4       1081.0       5.110       0.750         4       1081.0       5.110       0.750         5       865.0       5.100       0.740         6       721.0       5.100       0.740         7       618.1       5.100       0.740         8       541.0       5.095       0.735         10       433.0       5.095       0.735         10       433.0       5.090       0.730         12       361.0       5.085       0.725         16       271.0       5.085       0.725         16       271.0       5.080       0.720         20       217.0       5.075       0.715         21       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         50       87.4       5.030       0.675         50       87				
2       2161.0       5.120       0.750         4       1081.0       5.110       0.750         4       1081.0       5.110       0.750         5       865.0       5.100       0.740         6       721.0       5.100       0.740         7       618.1       5.100       0.740         8       541.0       5.095       0.735         10       433.0       5.095       0.735         10       433.0       5.090       0.730         12       361.0       5.085       0.725         16       271.0       5.085       0.725         16       271.0       5.080       0.720         20       217.0       5.075       0.715         21       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         50       87.4       5.030       0.675         50       87	1	4321.0	5.180	0.820
3       1441.0       5.110       0.750         4       1081.0       5.110       0.750         5       865.0       5.100       0.740         6       721.0       5.100       0.740         7       618.1       5.100       0.740         9       481.0       5.095       0.735         10       433.0       5.090       0.735         12       361.0       5.090       0.730         14       309.6       5.085       0.725         16       271.0       5.080       0.720         18       241.0       5.080       0.720         18       241.0       5.080       0.720         18       241.0       5.080       0.720         18       241.0       5.080       0.720         20       217.0       5.075       0.715         22       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.035       0.675         45       9				
4       1081.0       5.110       0.750         5       865.0       5.100       0.740         6       721.0       5.100       0.740         7       618.1       5.100       0.740         8       541.0       5.100       0.740         9       481.0       5.095       0.735         10       433.0       5.090       0.730         12       361.0       5.090       0.730         14       309.6       5.085       0.725         16       271.0       5.080       0.720         18       241.0       5.080       0.720         20       217.0       5.075       0.715         22       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.675         50       87.4				
5       865.0       5.100       0.740         6       721.0       5.100       0.740         7       618.1       5.100       0.740         8       541.0       5.100       0.740         9       481.0       5.095       0.735         10       433.0       5.090       0.730         12       361.0       5.090       0.730         14       309.6       5.085       0.725         16       271.0       5.080       0.720         20       217.0       5.080       0.720         20       217.0       5.075       0.715         21       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         45       97.5       5.020       0.660         60       73.0				
6       721.0       5.100       0.740         7       618.1       5.100       0.740         8       541.0       5.100       0.740         9       481.0       5.095       0.735         10       433.0       5.090       0.730         12       361.0       5.090       0.730         14       309.6       5.085       0.725         16       271.0       5.080       0.720         18       241.0       5.080       0.720         18       241.0       5.080       0.720         18       241.0       5.075       0.715         22       197.4       5.070       0.710         24       181.0       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7				
8       541.0       5.100       0.740         9       481.0       5.095       0.735         10       433.0       5.090       0.730         12       361.0       5.090       0.730         14       309.6       5.085       0.725         16       271.0       5.080       0.720         20       217.0       5.075       0.715         22       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.695         30       145.0       5.050       0.695         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.	6		5.100	0.740
9 481.0 5.095 0.735 10 433.0 5.090 0.730 112 361.0 5.090 0.730 114 309.6 5.085 0.725 16 271.0 5.080 0.720 18 241.0 5.080 0.720 20 217.0 5.075 0.715 22 197.4 5.070 0.710 24 181.0 5.060 0.700 26 167.2 5.060 0.700 28 155.3 5.055 0.695 30 145.0 5.050 0.690 35 124.4 5.040 0.680 40 109.0 5.035 0.675 45 97.0 5.035 0.675 50 87.4 5.030 0.670 55 79.5 5.020 0.660 60 73.0 5.020 0.660 60 73.0 5.020 0.660 60 73.0 5.020 0.655 90 49.0 5.035 0.675 80 55.0 5.010 0.655 90 49.0 5.035 0.675 100 44.2 5.000 0.640 110 40.3 5.000 0.640 120 37.0 5.005 0.645 100 44.2 5.000 0.640 110 40.3 5.000 0.640 120 37.0 5.005 0.645 100 44.2 5.000 0.640 120 37.0 5.005 0.645 100 44.2 5.000 0.640 120 37.0 5.005 0.645 100 49.0 5.005 0.645 100 49.0 5.005 0.645 100 49.0 5.005 0.645 100 49.0 5.005 0.645 100 49.0 5.005 0.645 100 49.0 5.005 0.645 100 40.3 5.000 0.640 110 40.3 5.000 0.640 120 37.0 5.000 0.		618.1	5.100	
10       433.0       5.090       0.730         12       361.0       5.090       0.730         14       309.6       5.085       0.725         16       271.0       5.080       0.720         18       241.0       5.080       0.720         20       217.0       5.075       0.715         22       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.695         30       145.0       5.050       0.695         31       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.	8	541.0	5.100	0.740
12       361.0       5.090       0.730         14       309.6       5.085       0.725         16       271.0       5.080       0.720         18       241.0       5.080       0.720         20       217.0       5.075       0.715         22       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.655         80       55.0       5.010       0.640         110       40.3       5.005       0.645         10       44.2		481.0	5.095	0.735
14       309.6       5.085       0.725         16       271.0       5.080       0.720         18       241.0       5.080       0.720         20       217.0       5.075       0.715         22       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         55       79.5       5.020       0.660         70       62.7       5.030       0.675         80       55.0       5.010       0.655         80       55.0       5.010       0.655         80       55.0       5.010       0.655         80       55.0       5.010       0.655         80       55.0       5.010       0.655         80       55.0       5.000       0.640         10       44.2 </th <th></th> <th>433.0</th> <th></th> <th></th>		433.0		
16       271.0       5.080       0.720         18       241.0       5.080       0.720         20       217.0       5.075       0.715         22       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.655         90       49.0       5.005       0.645         100       44.2       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         220       16.				
18       241.0       5.080       0.720         20       217.0       5.075       0.715         22       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.				
20       217.0       5.075       0.715         22       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         220       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.				
22       197.4       5.070       0.710         24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         220       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.				
24       181.0       5.060       0.700         26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.655         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.550         407       11.				
26       167.2       5.060       0.700         28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.				
28       155.3       5.055       0.695         30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         280       16.4       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         493       9.8				
30       145.0       5.050       0.690         35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8				
35       124.4       5.040       0.680         40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9<				
40       109.0       5.035       0.675         45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
45       97.0       5.035       0.675         50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
50       87.4       5.030       0.670         55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
55       79.5       5.020       0.660         60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
60       73.0       5.020       0.660         70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
70       62.7       5.015       0.655         80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
80       55.0       5.010       0.650         90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
90       49.0       5.005       0.645         100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
100       44.2       5.000       0.640         110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
110       40.3       5.000       0.640         120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
120       37.0       5.000       0.640         178       25.3       4.975       0.615         214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515				
214       21.2       4.975       0.615         280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515			5.000	0.640
280       16.4       4.935       0.575         307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515	178	25.3	4.975	0.615
307       15.1       4.930       0.570         360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515	214	21.2	4.975	0.615
360       13.0       4.920       0.560         407       11.6       4.910       0.550         449       10.6       4.900       0.540         493       9.8       4.890       0.530         546       8.9       4.875       0.515	280	16.4	4.935	0.575
407     11.6     4.910     0.550       449     10.6     4.900     0.540       493     9.8     4.890     0.530       546     8.9     4.875     0.515	307	15.1	4.930	0.570
44910.64.9000.5404939.84.8900.5305468.94.8750.515	360	13.0	4.920	
493       9.8       4.890       0.530         546       8.9       4.875       0.515	407			
546 8.9 4.875 0.515	449			
	493		4.890	0.530
598 8.2 4.870 0.510				
	598	8.2	4.870	0.510

AQUIFER TEST DATA

JOB #1293 WELL#: TW 1

CONST. Q Well type: Type of aquifer test: PUMPING Distance from pumping well:

Meas. point for w. l.'s: T.O.C. Pump on:
Elevation of Measuring Pt.:

Pump off:
Static Water Level:

OKIFICE WEIR Data type:

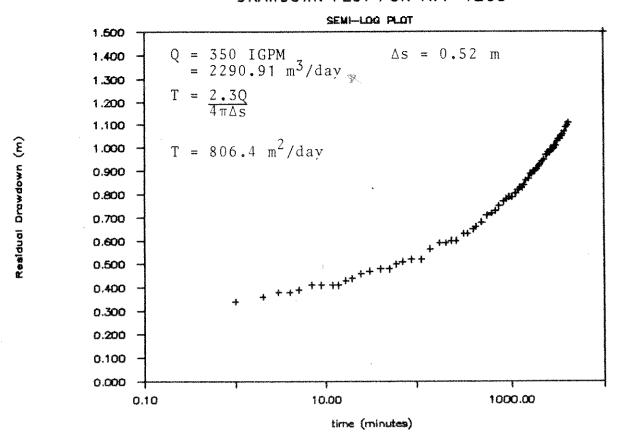
Depth pump:
Pump off:
4.36 Discharge rate How Q Measured: ORIFICE WEIR Data type: RECOVERY 18.3 m

07-10-87 16:00:00 10-10-87 16:00:00

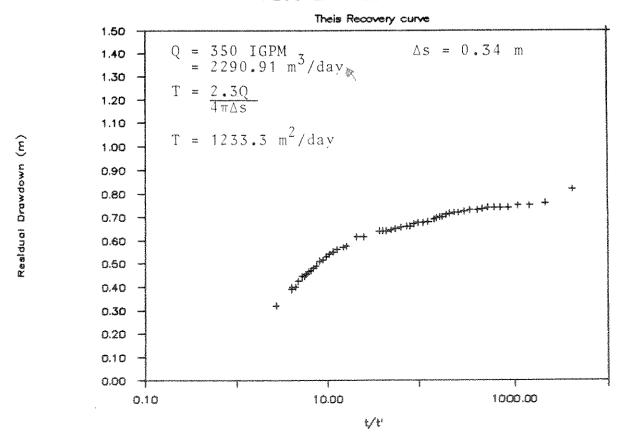
4.36 Discharge rate: 350 IGPM

At t' = 0, t =	4320 Wate	r Level Data	<b>1</b>
Time			Residual
minutes	t/t'	w.l. (m)	Drawdown
660	7.5	4.850	0.490
719	7.0	4.840	0.480
781	6.5	4.830	0.470
840	6.1	4.825	0.465
900	5.8	4.815	0.455
957	5.5	4.805	0.445
1016	5.3	4.805	0.445
1143	4.8	4,785	0.425
1259	4.4	4.760	0.400
1405	4.1	4.760	0.400
1440	4.0	4.750	0.390
2520	2.7	4.680	0.320
1440	4.0	4.750	0.390

#### DRAWDOWN PLOT FOR TW1-1293



### RECOVERY PLOT TW1-1293



JOB#1293 WELL#: TH87

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION How Q Measured: ORIFICE WEIR Data type: PUMPING How w. l.'s measured: W.L. TAPE Depth pump: 18.3 m Rad./dist. from pumping well:3.5 m Pump on: 07-10-87 16:00:00 Meas. point for w. l.'s(m): T.O.C. Pump off: 10-10-87 16:00:00 Ground Elevation (masl): Discharge rate: 350 IGPM Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION

Ground Elevation (masl): Discharge rate: 350 IG Static Water Level (m): 3.73 Length of Test: 72 HRS

Time from start of test (minutes)	W.L. reading (m)	Drawdown	Discharge rate Q (IGPM)	COMMENTS
6.0	3.860	0.130	350	
8.0	3.860	0.130		
10.0	3.880	0.150		
13.0	3.880	0.150		
15.0	3.890	0.160		
18.0	3.890	0.160		
21.0	3.900	0.170		
26.0	3.920	0.190		
30.0	3.920	0.190		
41.0	3.940	0.210		
51.0 61.0	3.940	0.210		
71.0	3.960	0.230		
89.0	3.970 3.980	0.240		
113.5	4.010	0.250		
143.5	4.020	0.280		
		0.290		
181.0	4.040	0.310		
210.0	4.060	0.330		
244.0	4.065	0.335		
300.0	4.070	0.340		
333.0	4.100	0.370		
364.5	4.090	0.360		
420.0	4.120	0.390		
448.0	4.130	0.400		
511.0	4.150	0.420		
573.0	4.170	0.440		
631.0	4.180	0.450		
694.0	4.190	0.460		
751.0	4.210	0,480		
841.0	4.230	0.500		
906.0 960.0	4.240 4.250	0.510 0.520		
1053.0	4.250	0.520		
	4.255			
1112.0 1176.0	4.280	0.525 0.550		
1232.0	4.290	0.560		
1232.0	4.290	0.560		
1354.0	4.300	0.570		
1412.0	4.315	0.570		
1528.0	4.330	0.600		

JOB#1293

WELL#: TH87

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION
How Q Measured: ORIFICE WEIR Data type: PUMPING
How w. 1.'s measured: W.L. TAPE Depth pump: 18.3 m

Rad./dist. from pumping well:3.5 m Pump on: 07-10-87 16:00:00 Meas. point for w. l.'s(m): T.O.C. Pump off: 10-10-87 16:00:00

Meas, point for W. 1. S(m): 1.0.0. Lamp 522.

Ground Elevation (masl): Discharge rate: 350 IGPM Static Water Level (m): 3.73 Length of Test: 72 HRS

from start of took	W.L. reading	Residual Discharge Drawdown rate	
from start of test (minutes)	(m)	s (m) Q (IGPM)	COMMENTS
1599.0	4.340	0.610	
1655.0	4.345	0.615	
1730.0	4.350	0.620	
1810.0	4.355	0.625	
1870.0	4.370	0.640	
1955.0	4.380	0.650	
2050.0	4.380	0.650	
2140.0	4.390	0.660	
2260.0	4.400	0.670	
2480.0	4.420	0.690	
2545.0	4.430	0.700	
2613.0	4.430	0.700	
2677.0	4.440	0.710	
2734.0	4.450	0.720	
2794.0	4.450	0.720	
2854.0	4.450	0.720	
2959.0	4.455	0.725	
3034.0	4.465	0.735	
3093.0	4.465	0.735	
3214.0	4.480	0.750	
3300.0	4.490	0.760	
3390.0	4.500	0.770	
3510.0	4.510	0.780	
3630.0	4.520	0.790	
3780.0	4.530	0.800	
3931.0	4.545	0.815	
4084.0 4219.0	4.550 4.565	0.820 0.835	

JOB #1293 WELL#: TH87

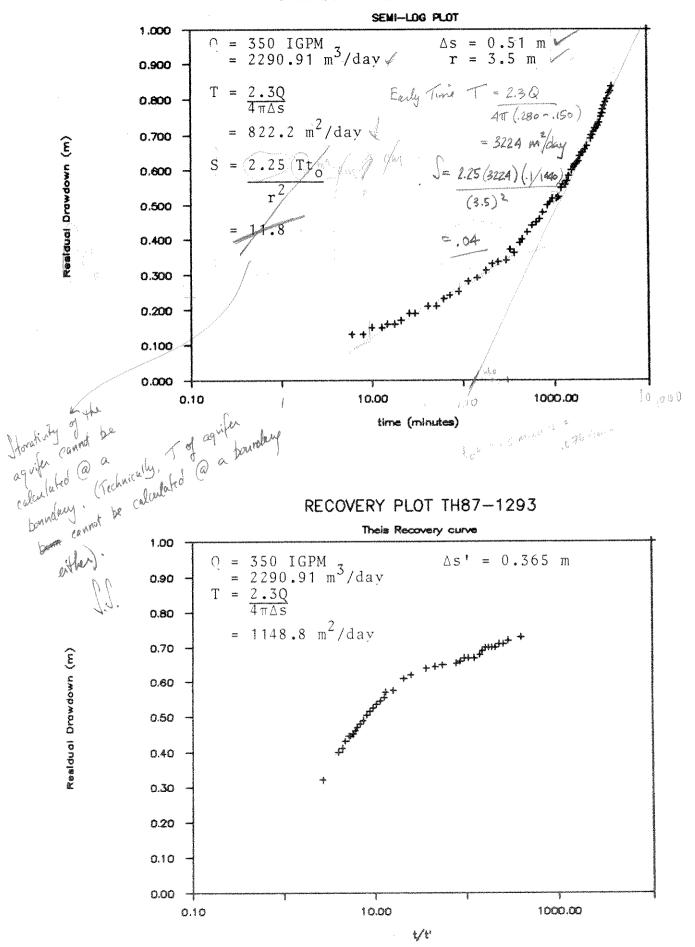
Type of aquifer test: CONST. Q Well type: OBSERVATION ORIFICE WEIR Data type: How Q Measured: RECOVERY Distance from pumping well:3.5 m Depth pump: 18.3 m

Meas. point for w. l.'s: T.O.C. Pump on: 07-10-87 16:00:00 10-10-87 16:00:00 Elevation of Measuring Pt.: Pump off:

Static Water Level: 3.73 Discharge rate: 350 IGPM

		• • • • • • • • • • • • • • • • • • • •		
At t' = 0, t =	4320	Water Level	Data	3
Time		,		Residual
minutes	t/t¹	w.l.	(m)	Drawdown
,				
11	393.7		.460	0.730
15	289.0		.450	0.720
17	255.1	4	.440	0.710
19	228.4	4	.440	0.710
21	206.7	4	.430	0.700
23	188.8	4	.430	0.700
25	173.8	4	.430	0.700
27	161.0	4	.430	0.700
29	150.0	4	.420	0.690
31	140.4	4	.410	0.680
36	121.0	4	.400	0.670
41	106.4	4	.400	0.670
46	94.9	4	.400	0.670
51	85.7	4	.390	0.660
56	78.1	4	.385	0.655
80	55.0		.380	0.650
96	46.0		.375	0.645
121	36.7		.370	0.640
179	25.1		.350	0.620
216	21.0		.340	0.610
283	16.3		.305	0.575
349	13.4		.300	0.570
364	12.9		.285	
409	11.6		.275	
451	10.6		.265	
494	9.7		.255	0.525
548	8.9		.245	
600	8.2		.235	
663	7.5		.220	
721	7.0		.210	0.480
783	6.5		.200	0.470
842	6.1	4	.190	0.460
901	5.8		.180	
960	5.5		.175	
1018	5.2		.175	
1143	4.8		.160	
1261	4.4		.140	0.410
1406	4.1		.130	
1440	4.0		.130	
2520	2.7		.050	
2320	ا « س <i>ا</i>	7		· · · · · · · ·

#### DRAWDOWN PLOT FOR TH87-1293



JOB#1293 WELL#: P72

Type of aquifer test: CONST.DISCHARGE Well type: **OBSERVATION** ORIFICE WEIR Data type: How Q Measured: How w. 1.'s measured: PUMPING 18.3 m

How w. 1.'s measured: W.L. TAPE Depth pump:
Rad./dist. from pumping well: 277.5 m Pump on:
Meas. point for w. 1.'s(m): T.O.C. Pump off:
Ground Flevation (magain) 07-10-87 16:00:00 10-10-87 16:00:00

Ground Elevation (masl): Discharge rate: 350 IGPM Static Water Level (m): 1.76 Length of Test: 72 HRS

from sta	Time art of test (minutes)	W.L. reading (m)	Drawdown	Discharge rate Q (IGPM)	COMMENTS
			9		
	73.0	1.790	0.030	350	
	107.0	1.840	0.080		
	135.0	1.860	0.100		
	166.0	1.870	0.110		
	232.0	1.890	0.130		
	301.0	1.905	0.145		
	412.0	1.925	0.165		
	470.0	1.950	0.190		
	532.0	1.955	0.195		
	645.0	1.960	0.200		
	722.0	1.970	0.210		
	855.0	1.970	0.210		
	930.0	1.980	0.220		
	1037.0	2.000	0.240		
	1161.0	2.010	0.250		
	1309.0	2.020	0.260		
	1435.0	2.040	0.280		
	1546.0	2.050	0.290		
	1669.0	2.060	0.300		
	1836.0	2.070	0.310		
	1988.0	2.080	0.320		
	2138.0	2.080	0.320		
	2400.0	2.090	0.330		
	2514.0	2.095	0.335		
	2634.0	2.110	0.350		
	2752.0	2.120	0.360		
	2861.0	2.125	0.365		
	2992.0	2.130	0.370		
	3119.0	2.140	0.380		
	3285.0	2.140	0.380		
	3400.0	2.150	0.390		
	3520.0	2.150	0.390		
	3640.0	2.160	0.400		
	3790.0	2.160	0.400		
	3952.0	2.170	0.410		
	4102.0	2.185	0.425		
	4236.0	2.190	0.430		

JOB #1293 WELL#: P72

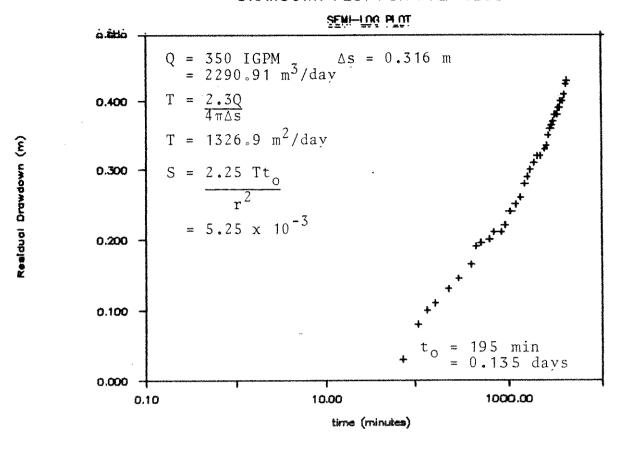
Type of aquifer test: CONST. Q Well type:
How Q Measured: ORIFICE WEIR Data type:
Distance from pumping well:277.5 m Depth pump: OBSERVATION RECOVERY 18.3 m

Meas. point for w. l.'s: T.O.C. Pump on: 07-10-87 16:00:00 Pump off: Elevation of Measuring Pt.: 10-10-87 16:00:00

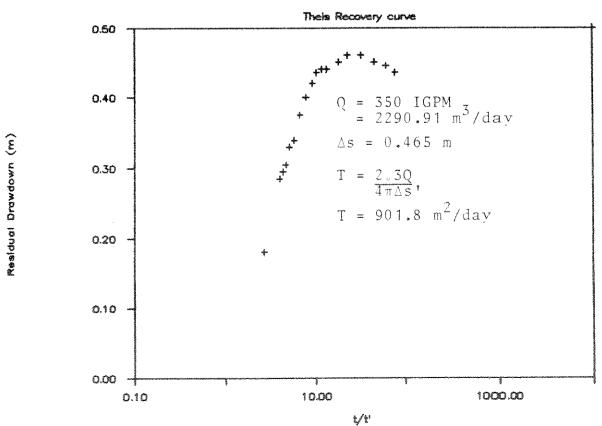
1.76 Discharge rate: 350 IGPM Static Water Level:

At $t' = 0$ , $t =$	4320 Wat	er Level Data	3
Time		•	Residual
minutes	t/t'	w.1. (m)	Drawdown
56	78,1	2.195	0.435
71	61.8	2.205	0.445
97	45.5	2.210	0.450
138	32.3	2.220	0.460
198	22.8	2.220	0.460
249	18.3	2.210	0.450
345	13.5	2.200	0.440
400	11.8	2.200	0.440
461	10.4	2.195	0.43
517	9.4	2.180	0.420
632	7.8	2.160	0.400
754	6.7	2.135	0.375
891	5.8	2.100	0.34
1046	5.1	2.090	0.330
1172	4.7	2.065	0.30
1289	4.4	2.055	0.29
1433	4.0	2.045	0.28
2547	2.7	1.940	0.180

## DRAWDOWN PLOT FOR P72-1293



# RECOVERY PLOT P72-1293



JOB#1293

WELL#: P75

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION
How Q Measured: ORIFICE WEIR Data type: PUMPING
How w. 1.'s measured: W.L. TAPE Depth pump: 18.3 m
Rad./dist. from pumping well:292 m Pump on: 07-10-87 16:00:00
Meas. point for w. 1.'s(m): T.O.C. Pump off: 10-10-87 16:00:00
Ground Elevation (masl): Discharge rate: 350 IGPM
Static Water Level (m): 3.38 Length of Test: 72 HRS

	Time	W.L.	Residual	Discharge	
from	start of test	reading	Drawdown	rate	COMMENTS
2	(minutes)	(m)		Q (IGPM)	CO::::D2::1D
	,			. ( ,	
	71.0	3.415	0.035	350	
	105.0	3.420	0.040		
	134.0	3.430	0.050		
	164.0	3.435	0.055		
	230.0	3.450	0.070		
	300.0	3.465	0.085		
	410.0	3.485	0.105		
	468.0	3.500	0.120		
	534.0	3.510	0.130		
	648.0	3.530	0.150		
	760.0	3.540	0.160		
	855.0	3.550	0.170		
	950.0	3.560	0.180		
	1027.0	3.580	0.200		
	1161.0	3.585	0.205		
	1308.0	3.610	0.230		
	1435.0	3.625	0.245		
	1676.0	3.640	0.260		
	1679.0	3.650	0.270		
	1847.0	3.670	0.290		
	2000.0	3.690	0.310		
	2140.0	3.700	0.320		
	2520.0	3.720	0.340		
	2632.0	3.740	0.360		
	2752.0	3.740	0.360		
	2871.0	3.750	0,370		
	2859.0	3.760	0.380		
	2991.0	3.780	0.400		
	3113.0	3.780	0.400		
	3285.0	3.790	0.410		
	3400.0	3.790	0.410		
	3520.0	3.810	0.410		
	3640.0	3.820	0.440		
	3810.0	3.830	0.450		
	3948.0	3.845	0.465		
	4100.0	3.850	0.470		
	4235,0	3.865	0.485		

JOB #1293 WELL#: P75

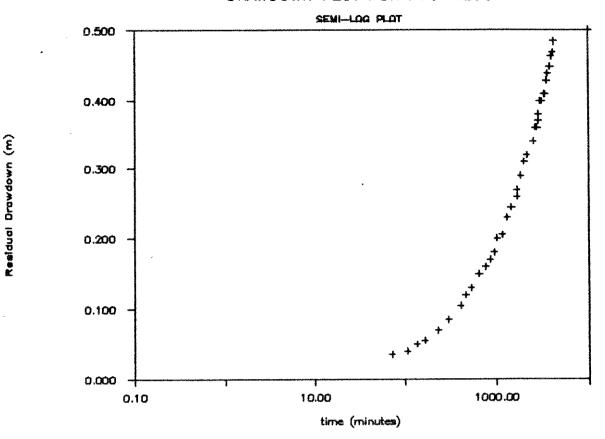
Type of aquifer test: CONST. Q Well type: OBSERVATION How Q Measured: ORIFICE WEIR Data type: RECOVERY 18.3 m

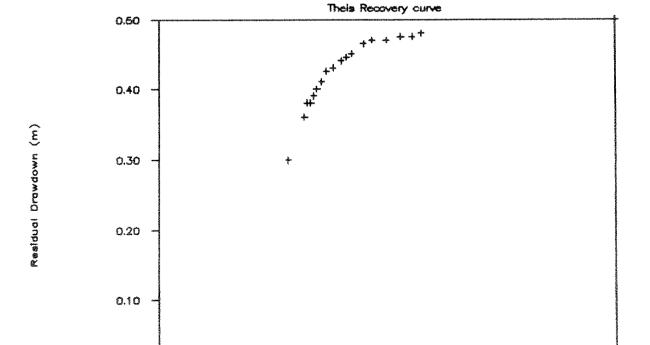
Distance from pumping well:292 m Depth pump:
Meas. point for w. l.'s: T.O.C. Pump on:
Elevation of Measuring Pt.: Pump off: 07-10-87 16:00:00

10-10-87 16:00:00 Static Water Level: 3.38 Discharge rate: 350 IGPM

$\mathbf{At} \ \mathbf{t'} = 0, \ \mathbf{t} =$	4320 Water	r Level Data	3
Time		*	Residual
minutes	t/t'	w.l. (m)	Drawdown
	T		
55	79.5	3.860	0.480
70	62.7	3.855	0.475
95	46.5	3.855	0.475
136	32.8	3.850	0.470
196	23.0	3.850	0.470
247	18.5	3.845	0.465
342	13.6	3.830	0.450
395	11.9	3.825	0.445
457	10.5	3.820	0.440
577	8.5	3.810	0.430
699	7.2	3.805	0.425
807	6.4	3.790	0.410
943	5.6	3.780	0.400
1032	5.2	3.770	0.390
1157	4.7	3.760	0.380
1274	4.4	3.760	0.380
1419	4.0	3.740	0.360
2535	2.7	3.680	0.300

## DRAWDOWN PLOT FOR P75-1293





10.00

t/t

0.00

0.10

RECOVERY PLOT P75-1293

1000.00

JOB#1293

WELL#: P79

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION
How Q Measured: ORIFICE WEIR Data type: PUMPING
How w. 1.'s measured: W.L. TAPE Depth pump: 18.3 m
Rad./dist. from pumping well:602 m Pump on: 07-10-87 16:00:00
Meas. point for w. 1.'s(m): T.O.C. Pump off: 10-10-87 16:00:00
Ground Elevation (masl): Discharge rate: 350 IGPM

Ground Elevation (masl):

Static Water Level (m):

Discharge rate: 350 1GF

2.19 Length of Test: 72 HRS

Time from start of test (minutes)	W.L. reading (m)	Residual Discharge Drawdown rate s (m) Q (IGPM)	COMMENTS
173.0 308.0 419.0 600.0 825.0 940.0 1170.0 1443.0 1687.0 1930.0 2160.0 2519.0 2760.0 2997.0 3555.0 3825.0	2.230 2.260 2.270 2.300 2.320 2.340 2.340 2.410 2.430 2.460 2.480 2.510 2.530 2.540 2.590 2.610	0.040 350 0.070 0.080 0.110 0.130 0.150 0.180 0.220 0.240 0.270 0.290 0.320 0.340 0.350 0.400 0.420	
4109.0 4243.0	2.630 2.635	0.440 0.445	

JOB #1293

WELL#: P79

Type of aquifer test: CONST. Q Well type: OBSERVATION How Q Measured: ORIFICE WEIR Data type: RECOVERY Distance from pumping well:602 m Depth pump: 18.3 m

Distance from pumping well:602 m Depth pump: 18.3 m

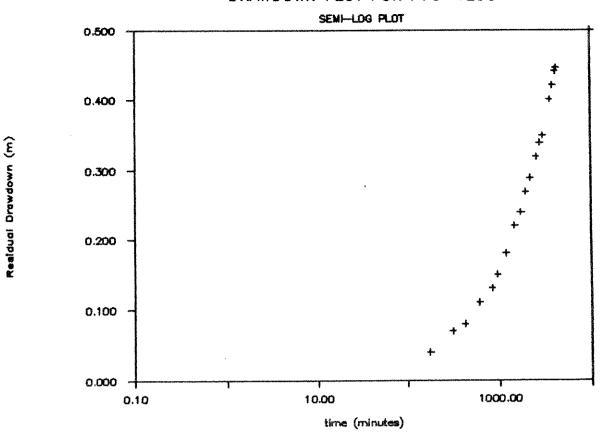
Meas. point for w. l.'s: T.O.C. Pump on: 07-10-87 16:00:00

Elevation of Measuring Pt.: Pump off: 10-10-87 16:00:00

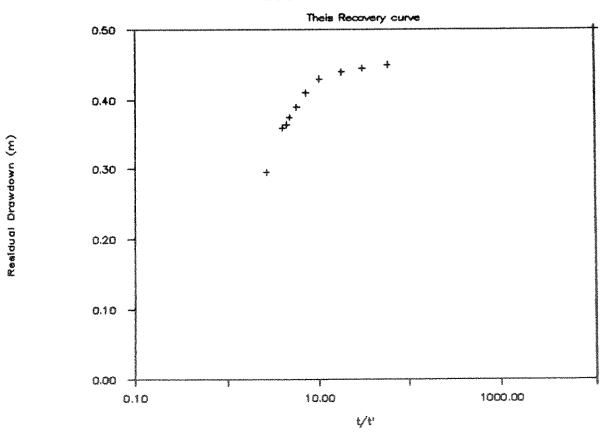
Static Water Level: 2.19 Discharge rate: 350 IGPM

At t' = 0, t =	4320 Wat	er Level Data	
Time			Residual
minutes	t/t'	w.1. (m)	Drawdown
76	57.8	2.640	0.450
147	30.4	2.635	0.445
254	18.0	2.630	0.440
473	10.1	2.620	0.430
702	7.2	2.600	0.410
934	5.6	2.580	0.390
1167	4.7	2.565	0.375
1284	4.4	2.555	0.365
1484	3.9	2.550	0.360
2598	2.7	2.485	0.295

## DRAWDOWN PLOT FOR P79-1293







JOB#1293

WELL#: P80

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION
How Q Measured: ORIFICE WEIR Data type: PUMPING
How w. l.'s measured: W.L. TAPE Depth pump: 18.3 m
Rad./dist. from pumping well:667 m Pump on: 07-10-87 16:00:00
Meas. point for w. l.'s(m): T.O.C. Pump off: 10-10-87 16:00:00

Ground Elevation (masl): Discharge rate: 350 IGE Static Water Level (m): 3.02 Length of Test: 72 HRS Discharge rate: 350 IGPM

Time from start of test (minutes)	W.L. reading (m)	Residual Discharge Drawdown rate COMMENTS s (m) Q (IGPM)	
178.0 312.0 423.0 605.0 830.0 935.0 1173.0 1446.0 1681.0 1920.0 2165.0 2522.0 2763.0 3001.0 3555.0 3825.0 4113.0	3.060 3.090 3.110 3.130 3.170 3.200 3.215 3.250 3.275 3.300 3.320 3.360 3.385 3.400 3.430 3.450 3.480	0.040 350 0.070 0.090 0.110 0.150 0.180 0.195 0.230 0.255 0.280 0.300 0.340 0.365 0.380 0.410 0.430 0.460	-
4246.0	3.490	0.470	

JOB #1293 WELL#: P80

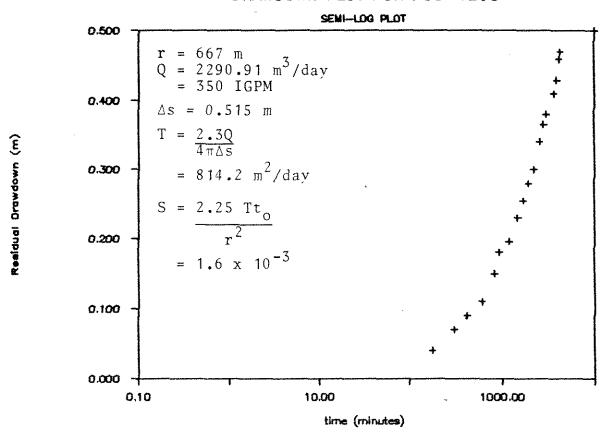
Type of aquifer test: CONST. Q Well type: OBSERVATION How Q Measured: ORIFICE WEIR Data type: RECOVERY Depth pump: 18.3 m

Distance from pumping well:667 m
Meas. point for w. l.'s: T.O.C.
Elevation of Measuring Pt.: Pump on: 07-10-87 16:00:00 10-10-87 16:00:00 Pump off:

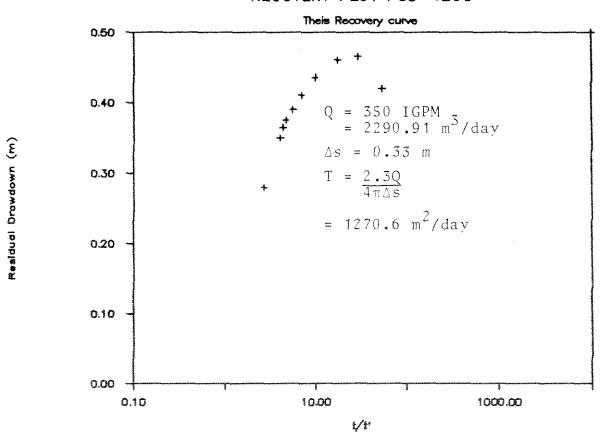
Static Water Level: 3.02 Discharge rate: 350 IGPM

At t' = 0, t =	4320 Wat	er Level Data	3
Time			Residual
minutes	t/t'	w.l. (m)	Drawdown
80	55.0	3.440	0.420
150	29.8	3.485	0.465
258	17.7	3.480	0.460
477	10.1	3.455	0.435
708	7.1	3.430	0.410
939	5.6	3.410	0.390
1170	4.7	3.395	0.375
1287	4.4	3.385	0.365
1431	4.0	3.370	0.350
2546	2.7	3.300	0.280

### DRAWDOWN PLOT FOR P80-1293



### RECOVERY PLOT P80-1293



AQUIFER TEST DATA JOB#1293 WELL#: P85

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION
How Q Measured: ORIFICE WEIR Data type: PUMPING
How w. l.'s measured: W.L. TAPE Depth pump: 18.3 m
Rad./dist. from pumping well:142 m Pump on: 07-10-87 16:00:00
Meas. point for w. l.'s(m): T.O.C. Pump off: 10-10-87 16:00:00
Ground Elevation (masl): Discharge rate: 350 IGPM

Ground Elevation (masl): Discharge rate: 350 IGI Static Water Level (m): 4.40 Length of Test: 72 HRS

Time W.L. Residual Discharge from start of test reading Drawdown rate COMM (minutes) (m) s (m) Q (IGPM)  3.0 4.400 0.000 350	ENTS
from start of test reading Drawdown rate COMM (minutes) (m) s (m) Q (IGPM)  3.0 4.400 0.000 350	ENTS
(minutes) (m) s (m) Q (IGPM)  3.0 4.400 0.000 350	
9.0 4.400 0.000	
12.0 4.400 0.000	:
15.0 4.400 0.000	
17.0 4.400 0.000	
20.0 4.400 0.000	
26.0 4.400 0.000	
31.0 4.400 0.000	
41.0 4.405 0.005	
51.0 4.405 0.005	
119.0 4.425 0.025	
150.0 4.430 0.030	
212.0 4.450 0.050	
272.0 4.455 0.055	
392.0 4.475 0.075	
453.0 4.475 0.075	
515.0 4.490 0.090	
595.0 4.500 0.100	
660.0 4.510 0.110	
760.0 4.530 0.130	
845.0 4.540 0.140	
910.0 4.550 0.150	
1048.0 4.570 0.170	
1145.0 4.560 0.160	
1295.0 4.585 0.185	
1423.0 4.605 0.205	
1523.0 4.610 0.210	
1624.0 4.630 0.230	
1827.0 4.640 0.240	
1962.0 4.660 0.260	
2103.0 4.670 0.270	
2245.0 4.680 0.280	
2380.0 4.690 0.290	
2498.0 4.700 0.300	
2618.0 4.715 0.315	
2738.0 4.720 0.320	
2844.0 4.730 0.330	
2977.0 4.740 0.340	
3099.0 4.750 0.350	
3275.0 4.760 0.360	

JOB#1293

WELL#: P85

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION

How Q Measured: ORIFICE WEIR Data type: PUMPING How w. 1.'s measured: W.L. TAPE Depth pump: 18.3 m

Rad./dist. from pumping well:142 m Pump on: 07-10-87 16:00:00 Meas. point for w. 1.'s(m): T.O.C. Pump off: 10-10-87 16:00:00

Ground Elevation (masl): Discharge rate: 350 IGPM Static Water Level (m): 4.40 Length of Test: 72 HRS

Time from start of test (minutes)	W.L. reading (m)	Residual Discharge Drawdown rate s (m) Q (IGPM)	COMMENTS
3390.0	4.770	0.370	
3510.0	4.780	0.380	
3630.0	4.790	0.390	
3780.0	4.800	0.400	
3935.0	4.815	0.415	
4088.0	4.825	0.425	
4223.0	4.830	0.430	

JOB #1293 WELL#: P85

Type of aquifer test: CONST. Q Well type: OBSERVATION
How Q Measured: ORIFICE WEIR Data type: RECOVERY
Distance from pumping well:142 m Depth pump: 18.3 m
Meas. point for w. l.'s: T.O.C. Pump on: 07-10-87 16:00:00
Elevation of Measuring Pt.: Pump off: 10-10-87 16:00:00

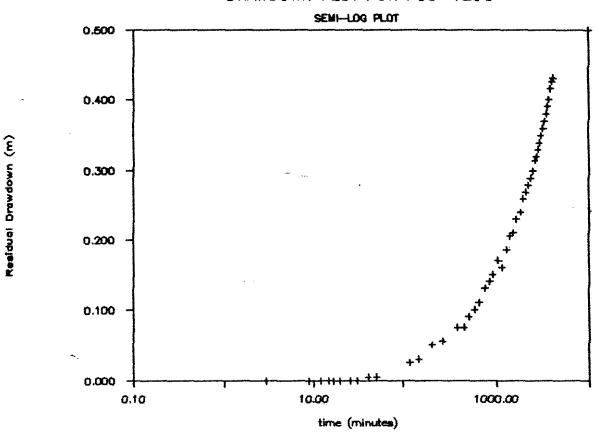
Meas. point rot w. ...

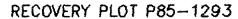
Elevation of Measuring Pt.: Pump orr:

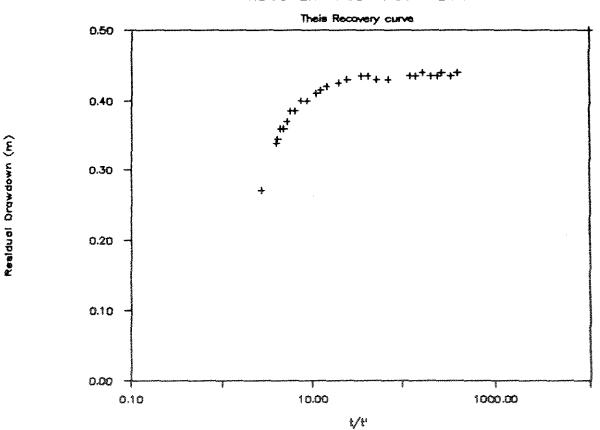
4.4 Discharge rate: 350 IGPM

	4333		<b></b>	
At t' = 0, t =	4320	Water Level	Data	
Time				Residual
minutes	t/t'	w.1.	(m)	Drawdown
11	393.7	Δ	. 840	0.440
13	333.3		835	0.435
16	271.0		.840	0.440
18	241.0		.835	0.435
			.835	0.435
21	206.7			
26	167.2		840	0.440
31	140.4		.835	0.435
36	121.0		.835	0.435
63	69.6		.830	0.430
85	51.8		.830	0.430
106	41.8		.835	0.435
126	35.3		.835	0.435
184	24.5		.830	0.430
232	19.6		.825	0.425
320	14.5		.820	0.420
375	12.5		.815	0.415
433	11.0		.810	0.410
554	8.8		.800	0.400
669	7.5		.800	0.400
789	6.5		.785	0.385
910	5.7		.785	0.385
1028	5.2	4	.770	0.370
1154	4.7	4	.760	0.360
1272	4.4	4	.760	0.360
1417	4.0	4	.745	0.345
1453	4.0	4	.740	0.340
2521	2.7	4	.670	0.270









JOB#1293 WELL#: P86

Type of aquifer test: CONST.DISCHARGE Well type:

How Q Measured: ORIFICE WEIR Data type: PUMPING
How w. 1.'s measured: W.L. TAPE Depth pump: 18.3 m

Rad./dist. from pumping well:105 m Pump on: 07-10-87 16:00:00
Meas. point for w. 1.'s(m): T.O.C. Pump off: 10-10-87 16:00:00

Discharge rate: 350 IGPM Ground Elevation (masl): Discharge rate: 350 IGI Static Water Level (m): 3.34 Length of Test: 72 HRS

Time from start of test (minutes)	W.L. reading (m)	Residual Disch Drawdown rat s (m) Q (IO	e COMMENTS
(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	\		
1.0	3.340	0.000 350	)
2.0	3.340	0.000	
5.0	3.360	0.020	
7.0	3.370	0.030	
10.0	3.370	0.030	
13.0	3.380	0.040	
16.0	3.380	0.040	
18.0 21.0	3.390 3.395	0.050 0.055	
25.0	3.400	0.060	
30.0	3.400	0.060	
35.0	3.400	0.060	
40.0	3.400	0.060	
45.0	3.405	0.065	
50.0	3.410	0.070	
117.0	3.440	0.100	
148.0	3.450	0.110	
209.0	3.470	0.130	
270.0	3.490	0.150	
390.0	3.510	0.170	
451.0	3.520	0.180	
508.0	3.530	0.190	
620.0	3.550	0.210	
670.0	3.550	0.210	
761.0	3.560	0.220	
846.0	3.580	0.240	
914.0	3.600	0.260	
1050.0 1143.0	3.620 3.630	0.280 0.290	
1293.0	3.650	0.310	
1421.0	3.665	0.325	
1524.0	3.680	0.340	
1630.0	3,695	0.355	
1825.0	3.740	0.400	
1960.0	3.740	0.400	
2100.0	3.740	0.400	
2240.0	3.760	0.420	
2385.0	3.770	0.430	
2425.0	3.800	0.460	
2495.0	3.780	0.440	

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION
How Q Measured: ORIFICE WEIR Data type: PUMPING
How w. 1.'s measured: W.L. TAPE Depth pump: 18.3 m
Rad./dist. from pumping well:105 m Pump on: 07-10-87 16:00:00
Meas. point for w. 1.'s(m): T.O.C. Pump off: 10-10-87 16:00:00

Meas. point ror w. r. -. -. Discharge race.

Ground Elevation (masl):

Discharge race.

3.34 Length of Test: 72 HRS Discharge rate: 350 IGPM

Time from start of test (minutes)	W.L. reading (m)	Residual Discharge Drawdown rate s (m) Q (IGPM)	COMMENTS
2617.0	3.785	0.445	
2739.0	3.795	0.455	
2842.0	3.800	0.460	
2975.0	3.810	0.470	
3098.0	3.820	0.480	
3260.0	3.830	0.490	
3390.0	3.840	0.500	
3510.0	3.850	0.510	
3630.0	3.860	0.520	
3780.0	3.870	0.530	
3933.0	3.890	0.550	
4086.0	3.900	0.560	
4221.0	3.905	0.565	

JOB #1293 WELL#: P86

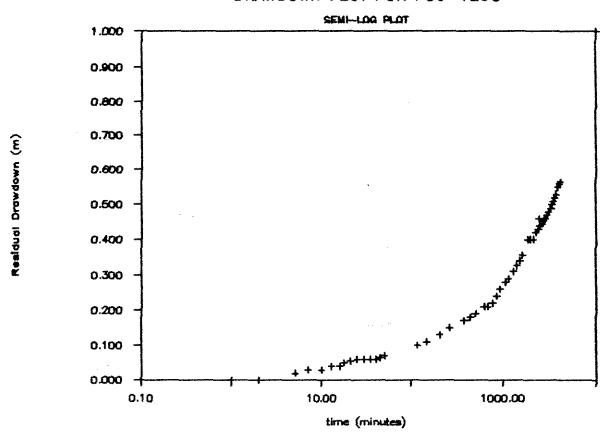
Type of aquifer test: CONST. Q Well type:
How Q Measured: ORIFICE WEIR Data type:
Distance from pumping well:105 m Depth pump:
T.O.C. Pump on: OBSERVATION RECOVERY 18.3 m

Distance from pumping well. T.O.C. Meas. point for w. 1.'s: T.O.C. 07-10-87 16:00:00 Elevation of Measuring Pt.: 10-10-87 16:00:00 Pump off:

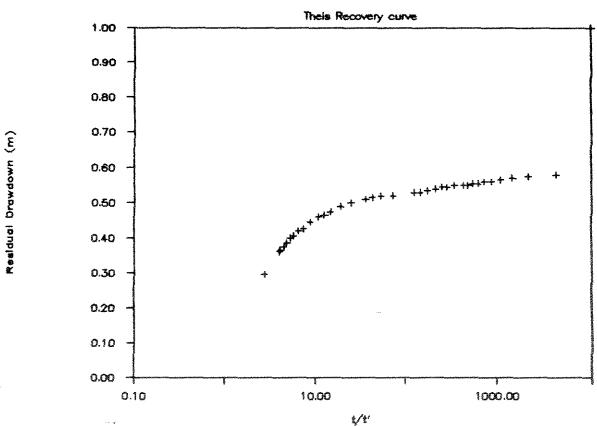
Static Water Level: 3.34 Discharge rate: 350 IGPM

At t' = 0, t =	4320	Water	Level	Data	3
Time		,			Residual
minutes	t/t'		w.1.	(m)	Drawdown
1	4321.0		3	.920	0.580
2	2161.0			.915	0.575
3	1441.0			.910	0.570
4	1081.0			.905	0.565
5	865.0			.900	0.560
6	721.0			.900	0.560
7	618.1			.895	0.555
8	541.0			.895	0.555
9	481.0			.890	0.550
10	433.0			.890	0.550
12.5	346.6			.890	0.550
15	289.0			.885	0.545
17	255.1			.885	0.545
20	217.0			.880	0.540
25	173.8			.875	0.535
30	145.0		3	.870	0.530
35	124.4		3	.870	0.530
61	71.8		3	.860	0.520
83	53.0		3	.860	0.520
104	42.5		3	.855	0.515
124	35.8		3	.850	0.510
181	24.9			.840	0.500
240	19.0			.830	0.490
314	14.8			.815	0.475
372	12.6			.805	0.465
430	11.0			.800	0.460
551	8.8			.785	0.445
666	7.5			.765	0.425
787	6.5			.760	0.420
908	5.8			.745	0.405
1020	5.2			.740	0.400
1146	4.8			.725	0.385
1264	4.4			.715	0.375
1409	4.1			.705	0.365
1451	4.0			.700	0.360
2519	2.7		3	.635	0.295

## DRAWDOWN PLOT FOR P86-1293







JOB#1293 WELL#: P88

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION ORIFICE WEIR Data type: How Q Measured: How w. l.'s measured: How Q Measured: PUMPING W.L. TAPE Depth pump: 18.3 m

Rad./dist. from pumping well:435 m Pump on: 07-10-87 16:00:00 Pump off: Meas. point for w. l.'s(m): T.O.C. 10-10-87 16:00:00

Ground Elevation (masl):

Discharge Later 172 HRS

3.66 Length of Test: 72 HRS Discharge rate: 350 IGPM

Time	W.L.	Residual Discharge	
from start of test	reading	Drawdown rate	COMMENTS
(minutes)	(m)	s (m) Q (IGPM)	
61.0	3.655	-0.005 350	
97.0	3.660	0.000	
125.0	3.675	0.015	
155.0	3.670	0.010	
219.0	3.675	0.015	
288.0	3.680	0.020	
398.0	3.695	0.035	
457.0	3.700	0.040	
522.0	3.705	0.045	
637.0	3.710	0.050	
781.0	3.710	0.050	
866.0	3.710	0.050	
966.0	3.720	0.060	
1016.0	3.720	0.060	
1150.0	3.720	0.060	
1298.0	3.730	0.070	
1426.0	3.735	0.075	
1536.0	3.740	0.080	
1669.0	3.745	0.085	
1840.0	3.760	0.100	
1990.0	3.760	0.100	
2130.0	3.760	0.100	
2395.0	3.770	0.110	
2501.0	3.780	0.120	
2622.0	3.785	0.125	
2741.0	3.795	0.135	
2847.0	3.805	0.145	
2980.0	3.810	0.150	
3103.0	3.820	0.160	
3280.0	3.830	0.170	
3390.0	3.830	0.170	
3510.0	3.840	0.180	
3630.0	3.850	0.190	
3780.0	3.860	0.200	
3938.0	3.850	0.190	
4091.0	3.860	0.200	
4226.0	3.870	0.210	

JOB #1293 WELL#: P88

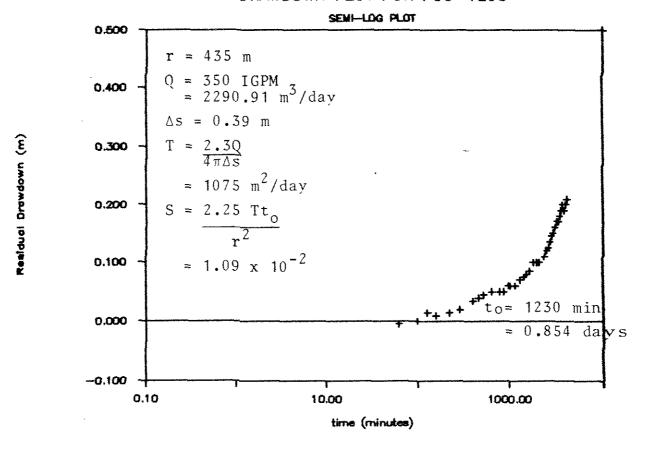
Type of aquifer test: CONST. Q Well type: OBSERVATION How Q Measured: ORIFICE WEIR Data type: RECOVERY Depth pump: Distance from pumping well:435 m 18.3 m

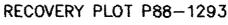
Meas. point for w. 1.'s: T.O.C. Pump on: 07-10-87 16:00:00 10-10-87 16:00:00 Elevation of Measuring Pt.: Pump off:

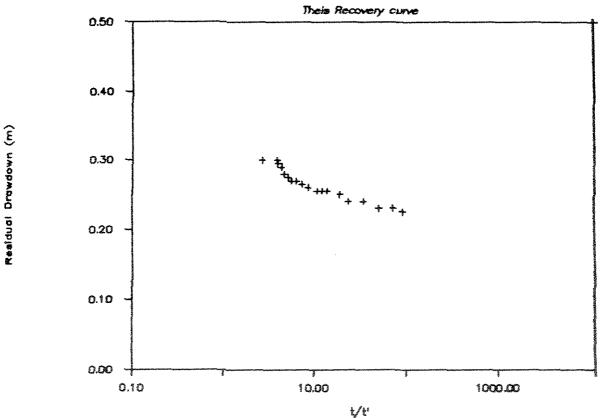
Static Water Level: 3.66 Discharge rate: 350 IGPM

At $t' = 0$ , $t =$	4320 Wat	er Level Dat	a
Time			Residual
minutes	t/t'	w.l. (m)	Drawdown
48	91.0	3.885	0.225
61	71.8	3.890	0.230
87	50.7	3.890	0.230
128	34.8	3.900	0.240
187	24.1	3.900	
234	19.5	3.910	0.250
330	14.1	3.915	0.25
380	12.4	3,915	0.25
438	10.9	3.915	0.25
559	8.7	3.920	0.26
673	7.4	3.925	0.26
794	6.4	3.930	0.27
914	5.7	3.930	0.27
1025	5.2	3.935	0.27
1151	4.8	3.940	0.28
1262	4.4	3.950	0.29
1415	4.1	3.955	0.29
1457	4.0	3.960	0.30
2524	2.7	3.960	0.30

### DRAWDOWN PLOT FOR P88-1293







JOB#1293

WELL#: P89

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION
How Q Measured: ORIFICE WEIR Data type: PUMPING
How w. l.'s measured: W.L. TAPE Depth pump: 18.3 m
Rad./dist. from pumping well: 450 m Pump on: 07-10-87 16:00:00
Meas. point for w. l.'s(m): T.O.C. Pump off: 10-10-87 16:00:00
Ground Elevation (masl): Discharge rate: 350 IGPM

Ground Elevation (masl):

Static Water Level (m):

Discharge rate: 350 IGE
4.58 Length of Test: 72 HRS

Time	W.L.	Residual Discharge	
from start of test	reading	Drawdown rate	COMMENTS
(minutes)	(m)	s (m) Q (IGPM)	
63.0	4.690	0.110 350	
98.0	4.715	0.135	
126.0	4.740	0.160	
157.0	4.755	0.175	
220.0	4.780	0.200	
290.0	4.800	0.220	
400.0	4.830	0.250	
460.0	4.845	0.265	
525.0	4.860	0.280	
635.0	4.880	0.300	
740.0	4.900	0.320	
865.0	4.920	0.340	
945.0	4.940	0.360	
1028.0	4.955	0.375	
1152.0	4.970	0.390	
1300.0	4.995	0.415	
1428.0	5.015	0.435	
1538.0	5.030	0.450	
1661.0	5.040	0.460	
1830.0	5.060	0.480	•
1980.0	5.070	0.490	
2130.0	5.090	0.510	
2395.0	5.110	0.530	
2503.0	5.125	0.545	
2623.0	5.130	0.550	
2743.0	5.135	0.555	
2849.0	5.140	0.560	
2982.0	5.150	0.570	
3105.0	5.165	0.585	
3280.0	5.180	0.600	
3390.0	5.190	0.610	
3510.0	5.200	0.620	
3630.0	5.210	0.630	
3780.0	5.220	0.640	
3940.0	5.230	0.650	
4093.0	5.230	0.650	
4228.0	5.250	0.670	

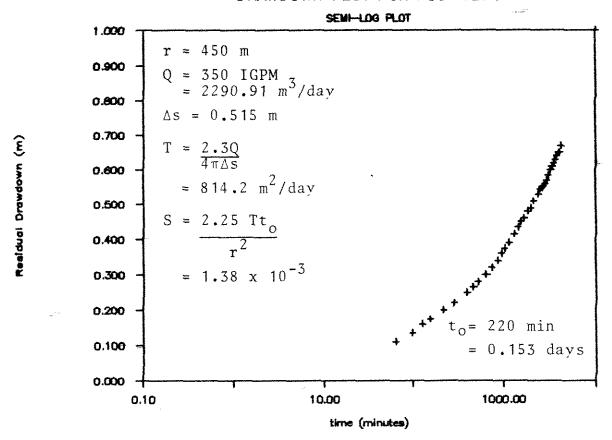
JOB #1293 WELL#: P89

Type of aquifer test: CONST. Q Well type: OBSERVATION
How Q Measured: ORIFICE WEIR Data type: RECOVERY
Distance from pumping well:450 m Depth pump: 18.3 m
Meas. point for w. l.'s: T.O.C. Pump on: 07-10-87 16:00:00
Elevation of Measuring Pt.: Pump off: 10-10-87 16:00:00

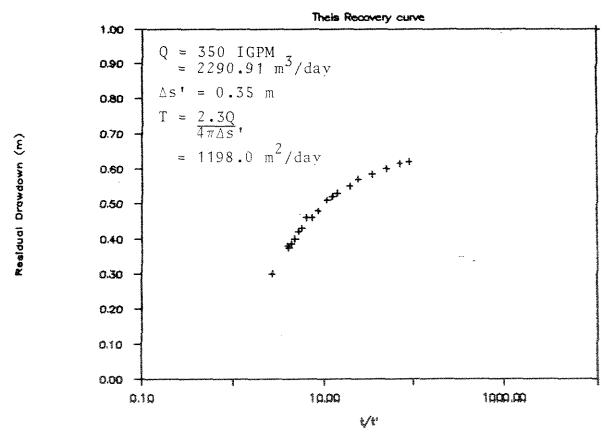
Elevation of Measuring Pt.: Pump off: 10-10-87
Static Water Level: 4.58 Discharge rate: 350 IGPM

At t' = 0, t =	4320 Water	Level Data	2
Time	20.00 00.00		- Residual
minutes	t/t'	w.l. (m)	
49	89.2	5.200	0.620
63	69.6	5.195	0.615
89	49.5	5.180	0.600
130	34.2	5.165	0.585
189	23.9	5.150	0.570
236	19.3	5.130	0.550
332	14.0	5.110	0.530
380	12.4	5.100	0.520
440	10.8	5.090	0.510
561	8.7	5.060	0.480
676	7.4	5.040	0.460
797	6.4	5.040	0.460
920	5.7	5.010	0.430
1027	5.2	5.000	0.420
1153	4.7	4.980	0.400
1270	4.4	4.965	0.385
1416	4.1	4.955	0.375
1458	4.0	4.960	0.380
2526	2.7	4.880	0.300

### DRAWDOWN PLOT FOR P89-1293



## RECOVERY PLOT P89-1293



JOB#1293 WELL#: P90

Type of aquifer test: CONST.DISCHARGE Well type: OBSERVATION How Q Measured:
How w. l.'s measured: ORIFICE WEIR Data type: PUMPING W.L. TAPE Depth pump: 18.3 m

07-10-87 16:00:00 Rad./dist. from pumping well:480 m Pump on: Pump off: Meas. point for w. l.'s(m): T.O.C. 10-10-87 16:00:00

Ground Elevation (masl): Discharge rate: 350 IGPM Static Water Level (m): 3.46 Length of Test: 72 HRS

Time from start of test (minutes)	W.L. reading (m)	Residual Discharg Drawdown rate s (m) Q (IGPM)	e COMMENTS
 64.0	3.460	0.000 350	·
94.0	3.465	0.005	
129.0	3.470	0.010	
160.0	3.470	0.010	
224.0	3.475	0.015	
294.0	3.480	0.020	
405.0	3.490	0.030	
483.0	3.500	0.040	
527.0	3.505	0.045	
632.0	3.510	0.050	
780.0	3.510	0.050	
864.0	3.510	0.050	
964.0	3.520	0.060	
1021.0	3.530	0.070	
1153.0	3.530	0.070	
1303.0	3.550	0.090	
1430.0	3.560	0.100	
1671.0	3.565	0.105	
1674.0	3.580	0.120	
1835.0	3.600	0.140	
1990.0	3.610	0.150	
2140.0	3.620	0.160	
2515.0	3.540	0.180	
2626.0	3.650	0.190	
2747.0	3.660	0.200	
2866.0	3.675	0.215	
2973.0	3.685	0.225	
3106.0	3.700	0.240	
3228.0	3.710	0.250	
3400.0	3.720	0.260	
3510.0	3.730	0.270	
3630.0	3.740	0.280	
3750.0	3.750	0.290	
3900.0	3.760	0.300	
3943.0	3.770	0.310	
4096.0	3.780	0.320	
4231.0	3.795	0.335	

JOB #1293 WELL#: P90

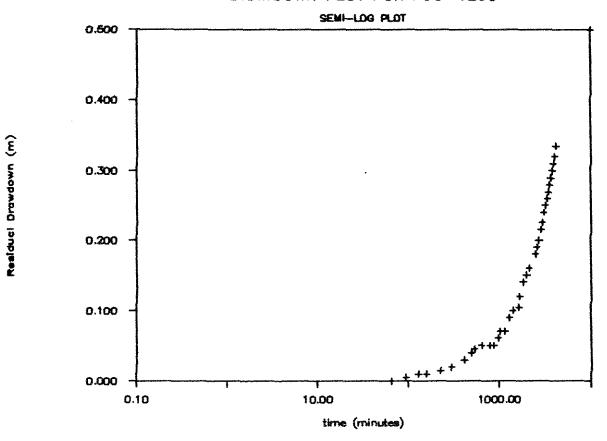
Type of aquifer test: CONST. Q Well type: OBSERVATION How Q Measured: ORIFICE WEIR Data type:
Distance from pumping well:480 m Depth pump:
Meas. point for w. l.'s: T.O.C. Pump on:
Elevation of Measuring Pt.: Pump off: RECOVERY 18.3 m

07-10-87 16:00:00 10-10-87 16:00:00

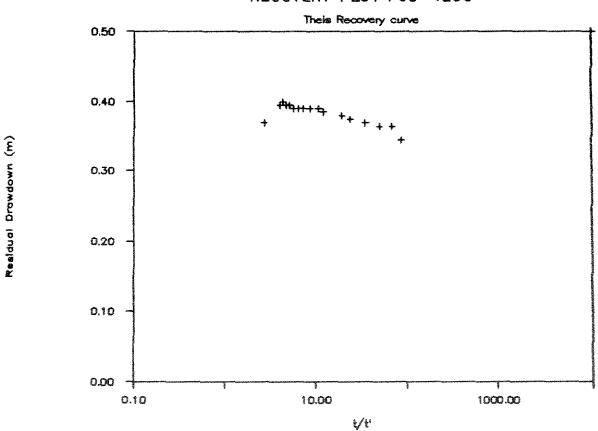
3.46 Discharge rate: 350 IGPM Static Water Level:

At t' = 0, t =	4320 Wat	er Level Data	3
Time			Residual
minutes	t/t'	w.l. (m)	Drawdown
51	85.7	3.805	0.345
66	66.5	3.825	0.365
91	48.5	3.825	0.365
132	33.7	3.830	0.370
192	23.5	3.835	0.37
239	19.1	3.840	0.380
388	12.1	3.845	0.38
445	10.7	3.850	0.39
560	8.7	3.850	0.39
682	7.3	3.850	0.39
800	6.4	3.850	0.39
927	5.7	3.850	0.39
1030	5.2	3.855	0.39
1156	4.7	3.855	0.39
1273	4.4	3.860	0.40
1418	4.0	3.855	0.39
2529	2.7	3.830	0.37









## Well Efficiency

$$T = \frac{2.3Q}{4\pi\Delta s}$$

$$T = 1000 \text{ m}^2/\text{day}$$

$$Q = 350 \text{ IGPM}$$
  
= 2290.91 m<sup>3</sup>/day

$$\Delta s = \frac{2.3Q}{4\pi T}$$

$$= \frac{2.3(2290.91)}{4\pi(1000)}$$

$$= 0.419 \text{ m}$$

actual drawdown from 72 hour test = 1.11 m

W.E. = 
$$\frac{\text{theoretical drawdown}}{\text{actual drawdown}}$$

$$= \frac{0.419}{1.11}$$

C-2 1990 Test Program

WELL#: 2314-TW1

ype of aquifer test:

Weir Data type:

Constant Q Well type:

Production

iow Q Measured:

)istance from pumping well: xxx

Depth pump:

Pumping 15.8 m

Meas. point for w. l.'s: T.O.C. Pump on:

Elevation of Measuring Pt.: xxx

Pump off:

03/05/90 19h00 06/05/90 19h00

Static Water Level:

3.47 Discharge rate: 350 igpm

Time	Water Level		-	Comments
(min.)	(m)	(m)	(i.g.p.m.)	
1.00	4.06	0.59	350.00	
2.00	4.08	0.61		
3.00	4.10	0.63		
4.00	4.11	0.64		
5.00	4.12	0.65		
6.00	4.13	0.66		
7.00	4.13	0.66		
8.00	4.14	0.67		
9.00	4.14	0.67		
10.00	4.15	0.68		
12.00	4.15	0.68		Pump off for 1 min
14.00	4.15	0.68		
16.00	4.15	0.68		
18.00	4.16	0.69		
20.00	4.17	0.70		Pump off for 1 min
25.00	4.17	0.70		
30.00	4.19	0.72		
35.00	4.22	0.75		
40.00	4.23	0.76		
45.00	4.22	0.75		Pump off for 1 min
50.00	4.22	0.75		
55.00	4.23	0.76		
60.00	4.25	0.78		
70.00	4.26	0.79		
80.00	4.28	0.81		
90.00	4.29	0.82		
105.00	4.30	0.83		
120.00	4.31	0.84		
180.00	4.32	0.85		
240.00	4.33	0,86		
300.00	4.35	0.88		
360.00	4.36	0.89		
420.00	4.38	0.91		
480.00	4.42	0.95		
540.00	4-42	0.95		
600.00	4.44	0.97		
660.00	4.46	0.99		
720.00	4.47	1.00		
780.00	4.50	1.03		
840.00	4.52	1.05		
900.00	4.54	1.07		

### WELL#: 2314-TW1

Type of aquifer test:

Constant Q Well type:

Production

How Q Measured:

Weir Data type: Pumping

Distance from pumping well: xxx

15.8 m

Meas, point for w. l.'s:

T.O.C.

03/05/90 19h00

Elevation of Measuring Pt.: xxx

Pump on: Pump off:

Depth pump:

06/05/90 19h00

Static Water Level:

3.47 Discharge rate: 350 igpm

	Time	Water Level	Drawdown	Discharge	Comments
	(min.)	(m)	(m)	(i.g.p.m.)	
	1020.00	4.55	1.08		-
	1080.00	4.56	1.09		
	1140.00	4.57	1.10		
	1200.00	4.58	1.11		
	1260.00	4.59	1.12		
•	1320.00	4.60	1.13		
	1380.00	4.60	1.13		
	1440.00	4.60	1.13		
	1500.00	4.60	1.13		
	1560.00	4.61	1.14		
	1620.00	4.61	1.14		
	1680.00	4.62			
	1740.00	4.63	1.16		
	1800.00	4.64	1.17		
	1860.00	4.66	1.19		
	1920.00	4.68	1.21		
	1980.00	4.70	1.23		
	2040.00	4.70	1.23		
	2100.00	4.71	1.24		
	2160.00	4-71	1.24		
	2220.00	4.71	1.24		
	2280.00	4.72	1.24		
	2340.00	4.71	1.24		
	2400.00	4.72	1.25		
	2460.00	4.73	1.26		
	2520.00	4.74	1.27		
	2580.00	4.75			
	2640.00	4.76			
	2700.00	4.77			
	2760.00	4.78			
	2820.00	4.78			
	2880.00	4.78			
	2940.00	4-80			
	3000.00	4.80			
	3060.00	4.80			
	3120.00	4-81			
	3180.00	4.82			
	3240.00	4.82			
	3300.00	4.82			
	3360.00	4.83			
	3420.00	4.84			
	3480.00	4.84			

WELL#: 2314-TW1

Type of aquifer test:

Constant Q Well type:

Production

How Q Measured:

Weir Data type: Pumping 15.8 m

Distance from pumping well: XXX

Depth pump: Pump on:

03/05/90 19h00

Meas. point for w. l.'s:

T.O.C.

Elevation of Measuring Pt.: XXX

Pump off:

06/05/90 19h00

Static Water Level:

3.47 Discharge rate: 350 igpm

Time	Water Level	Drawdown	Discharge Comments
(min.)	(m)	(m)	(i.g.p.m.)
3540.00	4.84	1,37	
3600.00	4.85	1.38	
3660.00	4.86	1.39	
372ó.00	4.87	1.40	
3780.00	4.88	1.41	
3840.00	4.88	1.41	
3900.00	4.88	1.41	
3960.00	4.88	1.41	
4020.00	4.89	1,42	
4080.00	4.90	1.43	
4140.00	4.90	1.43	
4200.00	4.90	1.43	
4260.00	4.90	1.43	
4320.00	4.90	1.43	

Type of aquifer test: Constant Q Well type: Observation Data type: How Q Measured: Pumping Weir

Depth well: 55 ft. T.O.C. Pump on:

Distance from pumping well: 2 m Meas. point for w. l.'s: T.O. Elevation of Measuring Pt.: xxx Static Water Level: 05-03-90 19h00 05-06-90 19h00 Pump off:

WELL#: 2314-0W87

3.18 Discharge rate: 350 igpm

Time (min.)	Water Level (m)	Drawdown (m)	Discharge (i.g.p.m.)
(1111.)	(1111)	(1111)	(1-g.p.m.)
2.25	3.28	0.10	350.00
3.25	3.29	0.11	350.00
4.50	3.30	0.12	350.00
14.00	3.33	0.15	350.00
15.00	3.35	0.17	350.00
16.00	3.35	0.17	350.00
22.00	3.37	0.19	350.00
25.00	3.37	0.19	350.00
31.00	3.39	0.21	350.00
33.00	3.40	0.21	350.00
34.00	3.40	0.21	350.00
40.00	3.41	0.23	350.00
49.00	3.43	0.24	350.00
60.00	3.44	0.26	350.00
94.00	3.49	0.31	350.00
108.00	3.49	0.31	350.00
404.00	3.60	0.42	350.00
730.00	3.70	0.52	350.00
1470.00	3.81	0.63	350.00
3284.00	3.98	0.80	350.00
4321.00	4.10	0.92	350.00

WELL#: 2314-0W84

Type of aquifer test: Observation Constant Q Well type: How Q Measured: Data type: Pumping Bucket

Distance from pumping well: app. 200 m Depth well: 55 ft.

Meas. point for w. l.'s: T.O. Elevation of Measuring Pt.: xxx Static Water Level: T.o.c. 05-03-90 Pump on: 19h00 Pump off: 05-06-90 19h00

3.94 Discharge rate: 350 IGPM

Time (min.)	Water Level (m)	Drawdown (m)	Discharge (i.g.p.m.)
9.50	3.94	0.00	350.00
103.00	3.94	0.00	350.00
413.00	3.94	0.00	350.00
726.00	3.94	0.00	350.00
1476.00	3.95	0.01	350.00
3290.00	3.97	0.03	350.00
4320.00	3.99	0.05	350.00

Constant Q Well type:
Bucket Data type:
142 m Depth well: Type of aquifer test: Observation How Q Measured: Pumping

Distance from pumping well: 142 m
Meas. point for w. l.'s: T.O.C.
Elevation of Measuring Pt.: xxx
Static Water Level: 55 ft. 05-03-90 Pump on: Pump off: 19h00 05-06-90 19h00

WELL#: 2314-0W85

3.82 Discharge rate: 350 IGPM

Time (min.)	Water Level (m)	Drawdown (m)	Discharge (i.g.p.m.)
7.75	3.82	0.00	350.00
19.00	3.83	0.01	350.00
28.00	3.83	0.01	350.00
37.00	3.84	0.02	350.00
46.00	3.84	0.02	350.00
100.00	3.86	0.04	350.00
412.00	3.92	0.10	350.00
725.00	3.98	0.16	350.00
1475.00	4.09	0.27	350.00
3289.00	4.25	0.43	350.00
4320.00	4.38	0.56	350.00

WELL#: 2314-OW89

Constant Q Well type: Bucket Data type: Type of aquifer test: Observation How Q Measured: Pumping

Depth well: 55 ft.

Distance from pumping well: 450 m Meas. point for w. 1.'s: T.O.C. Elevation of Measuring Pt.: xxx Static Water Level: T.O.C. Pump on: Pump off: 05-03-90 19h00 05-06-90 19h00

3.94 Discharge rate: 350 IGPM

Time (min.)	Water Level (m)	Drawdown (m)	Discharge (i.g.p.m.)
105.00	3.94	0.00	350.00
420.00	4.25	0.31	350.00
720.00	4.34	0.40	350.00
1480.00	4.45	0.51	350.00
3296.00	4.62	0.68	350.00
4320.00	4.72	0.78	350.00



#### MANN TESTING LABORATORIES LTD. 5550 McADAM ROAD, MISSISSAUGA, ONTARIO L4Z 1P1

PHONE: 890-2555 • TELEX: 06-960496

CUSTOMER: Water & Earth Science Associates

**REPORT #: 879021** 

Box 430 Carp, Ontario K0A 1L0

**CUSTOMER REF.#** 

ATTN:

Ms. Tami Sugarman

DATE SUBMITTED: Oct. 27/87

----- CERTIFICATE OF ANALYSIS

Sample Description:

WATER

Preparation:

Samples were prepared as recommended in APHA Standard methods for the examination of water and wastewater, 16th Edition, 1985 or MOE Handbook of analytical methods for environmental samples, 1983.

Note:

Additional information is available on request.

Methodology:

TOC -

combustion and I.R. detector

Chemical Results:

See Table 1.

DATE: Dec. 1, 1987

ROY G-SMITH, C.CHEM.

#### GEN-H

CLIENT: WATER AND EARTH SCIENCE ASSOCIATES LIMITED

REF. NO.: 879021

TABLE: 1

CHEMICAL ANALYSIS - GENERAL

CONC = mg/L UNLESS OTHERWISE NOTED

		1293	1293	1293				
	1	QA	/90			72 HRS	1	
	MDL				s-2	s-3		
CHEMICAL PARAMETERS	(mg/L)	EXPIT	TRUE				<u> </u>	
	1		 					
TOTAL ORGANIC CARBON	]   1	1	] []		6	6		
TOTAL ORGANIC CARDON	! ' !	i i	i ii			,		<b>!</b>
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Presence	1	l		ĺ				

MDL = INSTRUMENT/METHOD DETECTION LIMIT

NS = NON SUFFICIENT SAMPLE -- = NO ANALYSIS REQUIRED

b= EPA WP 386 c= NBS 1643b

d= EPA WP 1185+WS 378 MINERALS +N03/F-6

a= EPA WP 1083

e= OTHER

ICAP 19/7

TRACE METALS - 1

TRACE ELEMENTS IN WATER



### MANN TESTING LABORATORIES LTD. 5550 McADAM ROAD, MISSISSAUGA, ONTARIO L4Z 1P1

PHONE: 890-2555 • TELEX: 06-960496

February 12, 1988

Water & Earth Science Associates P.O. Box 430 Carp, Ontario KOA 1LO

Attention: Mr. Tami Sugarman

RE: PESTICIDE ANALYSIS

MANN #878958

Dear Mr. Sugarman:

Enclosed, please find the results of the analysis conducted on the samples received October 27, 1987.

An outline of the analytical methodology used in the analysis and copies of chromatograms are available upon request.

Should you have any further inquiries regarding these results, please do not hesitate to contact us directly.

Yours truly,

MANN TESTING LABORATORIES LTD.

Tim Munshaw, M.Sc., C.Chem. Manager, Environmental

Munshan

TM/jh Encl.



8958-1

REQ. #309 REPORT CONC. = ppb = ug/L WATER AND EARTH SCIENCE W.O. #878958

NITROGEN PHOSPHORUS	MDL	*	l	1293-	1293-	1293-
HERBICIDES	(ppb)	RECOVERY	BLANK	8-24 HR.	9-48 HR.	10-72 HR.
			· 			! 
ALDRIN	0.7	i šó		) 1		
DIELDRIN	0.7	92		 		 
ENDRIN	l   0.2 ,	90	••	 		 
CHLORDANE	7.0	91	••			**
DDT	30.0	92	**		 	••
HEPTACHLOR	] 3.0	90				••
HEPTACHLOR EPOXIDE	3.0	89	* *	**		••
LINDANE	4.0	88	- <del>-</del>			 
METHOXYCHLOR	100.0	91	* <del>-</del>		 1	••
PCB'S	3.0	98	+ <del>-</del>	• •	 	
TOXAPHENE	   5.0	93	••	- •		• •
CARBARYL	70.0	64	••	••	<b>-</b> -	
DIAZINON	2.0     2.0	87	**		   •• 	• • • • • • • • • • • • • • • • • • •
METHYL PARATHION	7.0	99	• •			
PARATHION	35.0	93		••	**	~ *

mdl = method detection limit
tr = trace amount detected

-- = NONE DETECTED



### MANN TESTING LABORATORIES LTD. 5550 McADAM ROAD, MISSISSAUGA, ONTARIO L4Z 1P1

PHONE: 890-2555 • TELEX: 06-960496

March 16, 1988

Water and Earth Science Associates Ltd. Box 430 Carp, Ontario KOA 1L0

Attention: Mr. Tami Sugarman

RE: REG 309 PESTICIDE ANALYSIS
REVISED REPORT
MANN #878958

Dear Mr. Sugarman:

Enclosed, please find the results of the analysis conducted on the samples received February 27, 1988.

An outline of the analytical methodology used in the analysis and copies of chromatograms are available upon request.

Should you have any further inquiries regarding these results, please do not hesitate to contact us directly.

Yours truly,

MANN TESTING LABORATORIES LTD.

Tim Munshaw, M.Sc., C.Chem. Manager, Environmental

Munshaw

TM/vs Encl.

#### REVISED REPORT

REQ. #309 REPORT CONC. = ppb = ug/L WATER AND EARTH SCIENCE

W.O. #878958

NITROGEN PHOSPHORUS	MOL	1 %	1	1293-	1293-	1293-
HERBICIDES	(ppb)	RECOVERY	BLANK	8-24 HR.	9-48 HR.	10-72 HR.
			 	 		1
ALDRIN	0.7	89	' 		t 	
					-	
DIELDRIN	0.7	92 	 	 I		**
ENDRIN	0.2	90	**			
						1
CHLORDANE	7.0	91 I	•• 	1 I	- <del></del>	\
DDT	30.0	92	+-	, 		
1150 T + 0111 OD	]   3.0				<u> </u>	1
HEPTACHLOR	] 3.0 	90 	**		~ <del>-</del>	
HEPTACHLOR EPOXIDE	3.0	89				
LINDANG	]   4.0	88		<b> </b>		 
LINDANE	4.0   	<b>0</b> 0	••			
METHOXYCHLOR	100.0	91	••			
PCB*S	   3.0	98		••	- <del>-</del>	1
PCB-5	J.0   	70				
TOXAPHENE	5.0	93			••	
2,4-0	   100.0	97				<del> </del> 
2,40	100.0	71	• •			1
2,4,5-TP (SILVEX)	10.0	95		••		
CARBARYL		64 l	~ •			
CARDARIL	'0.0	(4)   	7 7			1
DIAZINON	2.0	87			-+	• •
METHYL PARATHION		99 I	• •		~ ~	
DESTIL CANAIDIUM	, , , ,   	7 <b>7</b>				-
PARATHION	35.0	93	• •			

MDL = METHOD DETECTION LIMIT

-- = NONE DETECTED

MOL = METHOD DETECTION LIMIT

TR = TRACE AMOUNT DETECTED ANALYST: Fore Frozery is



Ministry Health

Ministère de la Santé

Services Branch

de Laboratoire

Date Received/ Date Reçue

Lab. No. / No. du Lab.

1207

## **Bacteriological Analysis of Water/**

Sample taken by/ Echantillon prélevé	par	ample taken by / Location of supply (t chantillon prélevé par Lieu de Prélèvemen			County	Date collected / Date du Prélèvemen
7-			1 1 11000	RMOC	(1) C   Cart   Cart	
four name and r	eturn address must :	appear on all copies	/ Votre nom et votre ad	resse de retou	r doivent paraît	Te sur foutes les coois
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	City, Town / Ville					
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	tizeris: check th		inking water only. S	See reverse	of report for	interpretation.
	s: cocher cette	case. Ea	u potable-seuleme	nt. Voir au v	erso pour in	terprétation.
Consult your	local health unit for	turther information	n./Pour les directives	additionel co	nsultez votre u	nité sanitaire local.
د SHAI ZON	DED AREAS FOR E OMBRÉE RÉSI	R OFFICIAL AGE ERVÉE AUX AGE	NCIES ONLY NTS OFFICIELS	within 6 ho	s samples MUS' urs if unrefriger refrigerated	ated or within
ZON	E OMBREE RESE	ERVÉE AUX AGE	NCIES ONLY NTS OFFICIELS COCHER TOUTES	within 6 hor 24 hours if	urs if unrefriger refrigerated.	ated or within
ZON	E OMBREE RESE	PRIATE BOXES /	NTS OFFICIELS	within 6 hor 24 hours if	urs if unrefriger refrigerated.	ated or within CEES
ZON	E OMBREE RESI CHECK APPROI	PRIATE BOXES /	COCHER TOUTES	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CEES
ZONI DRINKII  Treated	E OMBREE RESI CHECK APPROI NG WATER	PRIATE BOXES / NON-DRIN  Recreational	COCHEH TOUTES  KING WATER  Swimming Pool	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CEES
DRINKII	E OMBREE RESI CHECK APPROI NG WATER	PRIATE BOXES /	COCHEH TOUTES  KING WATER  Swimming Pool	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CEES
DRINKIN  Treated  Municipal	E OMBREE RESI CHECK APPROI NG WATER	PRIATE BOXES / NON-DRIN  Recreational Hydrotherapy Spa	COCHER TOUTES  KING WATER  Swimming Pool	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CEES
DRINKII  Treated	E OMBREE RESI CHECK APPROI NG WATER	PRIATE BOXES / NON-DRIN  Recreational Hydrotherapy	COCHER TOUTES  KING WATER  Swimming Pool	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CEES
DRINKII Treated Municipal	CHECK APPROING WATER  Non-treated	PRIATE BOXES / NON-DRIN  Recreational Hydrotherapy Spa	COCHER TOUTES  KING WATER  Swimming Pool	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CEES
DRINKIN  Treated  Municipal  Other Public  Single Housel	CHECK APPROING WATER  Non-treated  Noid	PRIATE BOXES / NON-DRIN Recreational Hydrotherapy Spa Other:	COCHEH TOUTES COCHEH TOUTES KING WATER Swimming Pool Sewage	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CEES
DRINKIN  Treated  Municipal  Other Public  Single Housel	CHECK APPROING WATER  Non-treated  Noid	PRIATE BOXES / NON-DRIN  Recreational Hydrotherapy Spa  Other:	COCHEH TOUTES COCHEH TOUTES KING WATER Swimming Pool Sewage BACTERIAL COUNT Based on, 1.0 mil	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CE
DRINKIN  Treated  Municipal  Other Public  Single Housel	CHECK APPROING WATER  Non-treated  Non-treated  Nolume / Base sur ui	PRIATE BOXES / NON-DRIN  Recreational Hydrotherapy Spa  Other:  BES BACTERIES In volume de 100 ml Faecal Strep /	COCHER TOUTES  COCHER TOUTES  KING WATER  Swimming Pool  Sewage	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CE
DRINKIN  Treated  Municipal  Other Public  Single Housel  ACTERIAL COUN ased on 100 ml v	CHECK APPROFING WATER  Non-treated  Non-treated  Nold  T / NUMERATION Dolume / Base sur units	PRIATE BOXES / NON-DRIN  Recreational  Hydrotherapy Spa  Other:  DES BACTÉRIES In volume de 100 mi	COCHEH TOUTES  COCHEH TOUTES  KING WATER  Swimming Pool  Sewage  BACTERIAL COUNT Based on 10 mill volume 7	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CE
DRINKIN  Treated  Municipal  Other Public  Single Housel  ACTERIAL COUN ased on 100 ml v	CHECK APPROFING WATER  Non-treated  Nold  T / NUMERATION Dolume / Base sur uit  Faecal Coliform/ Collibacilles	PRIATE BOXES / NON-DRIN  Recreational  Hydrotherapy Spa  Other:  DES BACTÉRIES TO Volume de 100 mi  Faecal Strep / Straptocoques	COCHEH TOUTES  COCHEH TOUTES  KING WATER  Swimming Pool  Sewage  BACTERIAL COUNT Based on 10 mill volume 7	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CE
DRINKIN  Treated  Municipal  Other Public  Single Housel  ACTERIAL COUN ased on 100 ml v	CHECK APPROFING WATER  Non-treated  Nold  T / NUMERATION Dolume / Base sur uit  Faecal Coliform/ Collibacilles	PRIATE BOXES / NON-DRIN  Recreational  Hydrotherapy Spa  Other:  DES BACTÉRIES TO Volume de 100 mi  Faecal Strep / Straptocoques	COCHEH TOUTES  COCHEH TOUTES  KING WATER  Swimming Pool  Sewage  BACTERIAL COUNT Based on 10 mill volume 7	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CE
DRINKIN  DRINKIN  Treated  Municipal  Other Public  Single Housel  ACTERIAL COUN ased on 100 ml v oral Coliform/ otale des colibacifies	CHECK APPROING WATER  Non-treated  Non-treated  Nolume / Base sur ui	PRIATE BOXES / NON-DRIN  Recreational  Hydrotherapy  Spa  Other:  ES BACTÉRIES n volume de 100 ml  Faecal Strep / Straptocoques Fecaux	COCHEH TOUTES  COCHEH TOUTES  KING WATER  Swimming Pool  Sewage  BACTERIAL COUNT Based on 10 mill volume 7	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CE
DRINKIN  DRINKIN  Treated  Municipal  Other Public  Single Housel  ACTERIAL COUN ased on 100 ml v oral Coliform/ otale des colibacifies	CHECK APPROING WATER  Non-treated  Non-treated  Nolume / Base sur ui	PRIATE BOXES / NON-DRIN  Recreational  Hydrotherapy  Spa  Other:  ES BACTÉRIES n volume de 100 ml  Faecal Strep / Straptocoques Fecaux	COCHEH TOUTES  KING WATER  Swimming Pool  Sewage  BACTERIAL COUNT Based on 10 mir volume APC	within 6 hor 24 hours if	urs if unrefriger refrigerated. S APPROPRI	ated or within CE

Ontario	Ministry of Health	Ministère de la Santé	Laboratory Services Branch	Service de Laboratoire		ate Received/ ate Reçue	Lab. No. / No. du Lab.
Omano			Bacteriologic Analyse Bac				9.1100
Sample take Echantilion			ocation of supply (Lot ieu de Prélèvement (l		ommune)	County	Date collected / Date du Prélèvement
少-			26, I	Gunte	iland	RMOC	Oct. 12/87
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	*	Province	- 1			Postal Code / Code	Postal (
Parti	iculiers:	ens: check this	ase. Eau	potable seule	ment. Voir a	se of report for au verso pour in	nterprétation.
						l consultez votre L table samples MUS	Inité sanitaire local.
60°C -	ZONE C	D AREAS FOR MBRÉE RÉSE	OFFICIAL AGEN RVÉE AUX AGEN	CIES ONLY ITS OFFICIELS	within 6	hours if unrefrigers if refrigers.	
	CH	IECK APPROP	RIATE BOXES / (	COCHER TOU	TES LES CA	SES APPROPR	IÉES
C	RINKING	WATER	NON-DRINK	ING WATER		COMME	NTS
☐ Treat	ted [	Non-treated	Recreational	Swimming Pool			
Muni	icipal		Hydrotherapy Spa	Sewage	<b>€</b>	787	
Othe	r Public		Other:				ੋਹ <u>ਵ</u> ਿੱ
Sing	le Househol	d	- La Caración de la C	·		-	9 F
		/ NUMERATION D ume / Base sur ur	ES BACTÉRIES 1 volume de 100 mt	BACTERIAL COUNT Based on 10 ml volume			
Total Colifor Totale des colibacilles	10	aecal Colligrm/ Collbacilles Fecaux	Faecal Strep./ Straptocoques Fecaux	APC			
Background	/   F	Paeruginosa	S aureus		_	- EO	

Date \$7, 10.14

Ontario	Ministry of Health	Ministère de la Santé	Laboratory Services Branch	Service de Laboratoire		Received/ Recue	Lab. No. No. du l	
•	ì			al Analysis d tériologique				
Sample take Echantillon //Succ			cation of supply (Lot, eu de Préjévement (L 26 / T	Con., Twp.)/ ot, Concession, Comm /CUMBER		RMOC	Date coll Date du l	ected / Prélèvement 8/87
Your name	and return ac	idress must app	ear on all copies / \	otre nom et votre ad	resse de retou	ır doivent paraîtı	re sur tout	es les copies.
	^	ne/Nom 1尺・ブ	BRAY			24		
٠	/	157 H	/Rue, R.R., Casier F ERON (		<b>ザ</b> /	**************************************	7.	
(د. <u>بر</u>	(	Town/Ville	WA		· Po	ostal Code / Code	Postal	
	.1	ONTAK	210		w	KIV &	<u> 383</u>	
Part	culiers: co	s: check this cher cette ca	ase. / Eau	king water only. S potable seuleme	ntVoir au	verso pour in	terpréta	tion.
Consu	SHADED	AREAS FOR	urther information. OFFICIAL AGEN RVÉE AUX AGEN	CIES UNLY -	Non potab within 6 h	onsultez votre u le samples MUS ours if unrefriger i refrigerated. F	The recei	ved To
-	CHE	CK APPROP	RIATE BOXES / (	COCHER TOUTE	S LES CASI	ES APPROPR	IÉES	
	RINKING W	ATER	NON-DRINK	ING WATER		COMME	TS.	
Trea	ted 🔲	Non-treated	Recreational	Swimming Pool				
	icipal		Hydrotherapy Spa	☐ Sewage		~		
OIM	r Public		Other:	20		3 1		
Sing	ie Household	5 : Carolin'	<u> </u>	****(**)		34 - 23	44	
BACTERI Based or	AL COUNT / N	UMERATION DI e / Base sur ur	S BACTÉRIES volume de 100 ml	BACTERIAL COUNT Based on 1.0 ml volume				
Total Colifo Totale des colibacille	Coli	cal Coliform/ bacilles aux	Faecal Strep./ Straptocoques Fecaux	APC .				
Backgroun	d Pae	ruginosa	S.eureus		36	\$	6.74	
Technician		/	Checked by	#11	Desa 77.10	)./4		G
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### MICROBIAL MONITORING REPORT

NSTITUTION WATE	R & EARTH SCIENCES	_
DATE COLLECTED		_
DATE REPORTED_	15-10-87	_
TECH SIGNATURE	•	
PHONED		

NO	SITE D	ESCRIPTION		LABORATO	RY REPOR	<b>-T</b>	
LAB #	WATER ANALYSIS:	as per water drinking	TOTAL	TOTAL	FAECAL	FAECAL	
	standards	*	COUNT	COLIFORM	COLIFORM	STREPT.	
WESA	2202 30 00 02	37 POND					
#1	1293 12/10/87 POND	2001/ml	53col/100ml	absent	absent		
WESA							
#2	72 hrs 1293	12/10/87	0col/ml	001/100ml	absent	absent	
			Townson Anna Anna Anna Anna Anna Anna Anna An				
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							20.00000 <b>年间的表现的时间</b> 10.00000000000000000000000000000000000

KEY:

NG = No Growth

NSG = No Significant Growth

NFL = Normal Flora

CC = Colony Count

NP = Non pathogenic

PP = Potential pathogen

MG = Mixed growth non-pathogenic and potential pathogens

DRINKING WATER: TT = Total Count

TC = Total Coliform

FC = Faecal Coliform

FS = Faecal Strept.

The results contained in this report are only representative of the sample(s) received by our laboratory. Interpretation of the results should include a consideration of the integrity of both the sampling technique and protocol.



### MICROBIAL MONITORING REPORT

INSTITUTION Water & Earth Science Association DATE COLLECTED set up 9-10-87 DATE REPORTED 13-10-87 TECH SIGNATURE

	* as per drinking water standa	ırds				PHONED
NO	SITE DESCRIPTION		ABORATO	RY REPOR	π	NOTES
LAB		Total Count	Total	Faecal	Faecal	
井	Water Analysis		Coliform	Coliform	Strept.	
WESA		2 col/ml	0 col/ml	absent	absent	the state of the s
#3	24 hours. 1293. 8/10/87					
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KEY:

NG = No Growth

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TC = Total Coliform

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The results contained in this report are only representative of the sample(s) received by our laboratory. Interpretation of the results should include a consideration of the integrity of both the sampling technique and protocol. A 0.0005514219 SHEET

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lc'd Const.	Const.	precip.	precip.	mg/L 3			
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	7.65E-04	7.65E-04	5.51E-04	3			
	2.41E-04	2.41E-04	2.41E-04	Dolomite 3			
atm)*	1.67E-03	1.67E-03	1.67E-03	0 3			
CO3)3.01E-03	3.01E-03	3.01E-03	2.74E-03	3			
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K1)*	7.74			3			
K2)*	-2.13			, ' 3			
K3)*	-4.27		adj. T(C) =	0 3			
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+ H20 = H+	+ HCO3-: I	K1	pH(s) =	8.02 3			
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eter	Value		Parameter	Value	PH	5	3
mg/L)	195.00		A	0.10			3 3
ess (CaCO3)	137.70		С	1.74		7.86	3
(CaCO3)	163.00		D	2.22			3
rature (C)	8.00	8	В	2.42			3
	8.00						3
	0.50						3
	0.05						3
	20	*	******	****	*****	****	3
6>R.I.>7 cor	rosion	~> *	Ryznar Ind	ex =	7.7	*	3
		*			4.	*	3
gical Incrus.	if:	*	rH =		16.72	*	3
> 0.3 mg/L,		*	*****	******	******	***	3
>-10 mV +/- 20							3
> 14.5 +/- 1	Thes	e co	nditions ap	ply to a w	vell being	pumped	3
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D-2 1990 Test Program

## ARECO CANADA INC.

APPLIED RESEARCH DIVISION

28 CONCOURSE GATE
NEPEAN, ONTARIO
CANADA K2E 7T7
TEL. (613) 228-1145
FAX. (613) 228-1148

CUSTOMER: WATER & EARTH SCIENCE ASSCUSTOMER REF. #: Vars Water Supply

ATTN: ROGER WOELLER

ORDER REF. #: 2314

REPORT #: 3151405

SAMPLE RECEIVED: May 4/90 and May 7/90

DATE SUBMITTED: May 14/90 & May 24/90

### CERTIFICATE OF ANALYSIS

SAMPLE DESCRIPTION:

VARS WATER SUPPLY - 2314-TW1

ANALYSIS PERFORMED:

**VARIOUS** 

**INSTRUMENTATION:** 

**VARIOUS** 

**RESULTS:** 

SEE ATTACHED

CERTIFIED BY Greg Clarkin

### WATER QUALITY ANALYSIS

### ARECO CANADA INC. 28 CONCOURSE GATE, NEPEAN, ONTARIO K2E 7T7

Lab. Number Sample I.D. Clients Job Number	040590-1A 2314-TW1-1HR. WESA P.O.#17773	
DETERMINATION	DETECTION	RESULTS
Colour (true) Hardness (CaCO <sub>3</sub> ) Alkalinity (CaCO <sub>3</sub> ) Turbidity Conductivity pH Chloride Fluoride Sulphate Nitrate (N) Nitrite (N) Calcium Sodium Ammonia (N) Potassium Iron Manganese Magnesium Hydrogen sulphide Phenols Total Nitrogen (TKN) Tannin/Lignin TOC DOC BOD Silica Coliform Count Fecal Count Fecal Strept. Background Uranium	1.0 TCU 0.05 mg/l 1.0 mg/l 1.0 NTU uS/cm 0.00 units 0.01 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.07 mg/l 0.09 mg/l 0.09 mg/l 0.09 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.1 mg/l 0.1 mg/l 1 mg/l 1 mg/l 1 mg/l 0.01 mg/l	25 128 175 6 340 7.84 4.18 <0.05 3.21 <0.05 <0.05 38.8 22.4 <0.05 3.02 0.738 0.056 7.73 0.107 <0.002 <0.1 
Cation Sum Anion Sum % Difference Ion Ratio TDS (ion sum calculated) Conductivity (calc.) SAR	meq/l meq/l % mg/l umho/cm	3.62 3.68 0.81 1.02 219 350 0.86

Lab Number Sample I.D. Clients Job Number	040590-1A 2314-TW1-1HR. WESA P.O.#1777	3
DETERMINATION	DETECTION (mg/L)	RESULTS (mg/L)
Benzene	0.002	<0.002
Toluene	0.002	<0.002
Ethylbenzene	0.002	<0.002
m,p-Xylene	0.002	<0.002
o-Xylene	0.002	<0.002

### WATER QUALITY ANALYSIS

### ARECO CANADA INC. 28 CONCOURSE GATE, NEPEAN, ONTARIO K2E 7T7

Lab. Number Sample I.D. Clients Job Number	040590-1B 2314-TW1-6HR. WESA P.O.#17773	
DETERMINATION	DETECTION	RESULTS
Colour (true) Hardness (CaCO <sub>3</sub> ) Alkalinity (CaCO <sub>3</sub> ) Turbidity Conductivity pH Chloride Fluoride Sulphate Nitrate (N) Nitrite (N) Calcium Sodium Ammonia (N) Potassium Iron Manganese Magnesium Hydrogen sulphide Phenols Total Nitrogen (TKN) Tannin/Lignin TOC DOC BOD Silica Coliform Count Fecal Count Fecal Strept. Background Uranium	1.0 TCU 0.05 mg/l 1.0 mg/l 1.0 NTU uS/cm 0.00 units 0.01 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.07 mg/l 0.09 mg/l 0.09 mg/l 0.09 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.1 mg/l 0.1 mg/l 0.1 mg/l 0.1 mg/l 0.01 mg/l	21
Cation Sum Anion Sum % Difference Ion Ratio TDS (ion sum calculated) Conductivity (calc.) SAR	meq/l meq/l % mg/l umho/cm	- - - -

Lab Number Sample I.D. Clients Job Number	040590-1B 2314-TW1-6HR. WESA P.O.#17773	3
DETERMINATION	DETECTION (mg/L)	RESULTS (mg/L)
Benzene	0.002	<0.002
Toluene	0.002	<0.002
Ethylbenzene	0.002	<0.002
m,p-Xylene	0.002	<0.002
o-Xylene	0.002	<0.002

### WATER QUALITY ANALYSIS

### ARECO CANADA INC. 28 CONCOURSE GATE, NEPEAN, ONTARIO K2E 7T7

Lab. Number Sample I.D. Clients Job Number	040590-1C 2314-TW1-12HR. WESA P.O.#17773	
DETERMINATION	DETECTION	RESULTS
Colour (true) Hardness (CaCO <sub>3</sub> ) Alkalinity (CaCO <sub>3</sub> ) Turbidity Conductivity pH Chloride Fluoride Sulphate Nitrate (N) Nitrite (N) Calcium Sodium Ammonia (N) Potassium Iron Manganese Magnesium Hydrogen sulphide Phenols Total Nitrogen (TKN) Tannin/Lignin TOC DOC BOD Silica Coliform Count Fecal Count Fecal Strept. Background Uranium	1.0 TCU 0.05 mg/l 1.0 mg/l 1.0 NTU uS/cm 0.00 units 0.01 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.07 mg/l 0.09 mg/l 0.09 mg/l 0.00 mg/l 0.01 mg/l 0.00 mg/l 0.00 mg/l 0.01 mg/l 0.02 mg/l 0.01 mg/l 0.01 mg/l 0.01 mg/l 0.01 mg/l 0.1 mg/l 0.1 mg/l 1 mg/l 1 mg/l 1 mg/l 1 mg/l 1 mg/l 0.01 mg/l 0.01 mg/l 0.01 mg/l 0.01 mg/l 0.1 mg/l 1 mg/l 1 mg/l 1 mg/l 0.01 mg/l	23 -6
Cation Sum Anion Sum % Difference Ion Ratio TDS (ion sum calculated) Conductivity (calc.) SAR	meq/l meq/l % mg/l umho/cm	

Lab Number Sample I.D. Clients Job Number	040590-1C 2314-TW1-12HR. WESA P.O.#17773	
DETERMINATION	DETECTION (mg/L)	RESULTS (mg/L)
enzene	0.002	<0.002
Toluene	0.002	<0.002
Ethylbenzene	0.002	<0.002
m,p-Xylene	0.002	<0.002
o-Xylene	0.002	<0.002

### WATER QUALITY ANALYSIS

### ARECO CANADA INC. 28 CONCOURSE GATE, NEPEAN, ONTARIO K2E 7T7

Lab. Number Sample I.D. Clients Job Number	070590-2A 2314-TW1-24HR. WESA P.O.#17773	
DETERMINATION	DETECTION	RESULTS
Colour (true) Hardness (CaCO <sub>3</sub> ) Alkalinity (CaCO <sub>3</sub> ) Turbidity Conductivity pH Chloride Fluoride Sulphate Nitrate (N) Nitrite (N) Calcium Sodium Ammonia (N) Potassium Iron Manganese Magnesium Hydrogen sulphide Phenols Total Nitrogen (TKN) Tannin/Lignin TOC DOC BOD Silica Coliform Count Fecal Count Fecal Strept. Background Uranium	1.0 TCU 0.05 mg/l 1.0 mg/l 1.0 NTU uS/cm 0.00 units 0.01 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.01 mg/l 0.00 mg/l 0.00 mg/l 0.01 mg/l 0.02 mg/l 0.01 mg/l 0.02 mg/l 0.01 mg/l 0.01 mg/l 0.1 mg/l 0.1 mg/l 0.1 mg/l 0.1 mg/l 0.1 mg/l 0.1 mg/l 0.1 mg/l 0.01 mg/l	25 - - 5 - - - - 0.716 - - 0.067 - - 6 - - - - - - - - - - - - - - - -
Cation Sum Anion Sum % Difference Ion Ratio TDS (ion sum calculated) Conductivity (calc.) SAR	meq/l meq/l % mg/l umho/cm	

Lab Number Sample I.D. Clients Job Number	070590-2A 2314-TW1-24HR. WESA P.O.#1777:	3
DETERMINATION	DETECTION (mg/L)	RESULTS (mg/L)
Benzene	0.002	<0.002
Toluene Ethylbenzene	0.002 0.002	<0.002 <0.002
m,p-Xylene	0.002	<0.002
o-Xylene	0.002	<0.002

Lab Number Sample I.D. Clients Job Number	070590-2C 2314-TW1-24HR. WESA P.O.#17774	
DETERMINATION	DETECTION (mg/L)	RESULTS (mg/L)
Benzene Bromodichloromethane Bromoform Bromomethane Carbon tetrachloride Chlorobenzene Chloroethane 2-Chloroethylvinyl ether Chloroform Chloromethane Dibromochloromethane 1,2-Dichlorobenzene 1,3-Dichlorobenzene 1,4-Dichlorobenzene 1,2-Dichloroethane 1,1-Dichloroethylene trans-1,2-Dichloroethylene trans-1,2-Dichloropropane cis-1,3-Dichloropropene trans-1,3-Dichloropropene trans-1,3-Dichloropropene Ethylbenzene Methylene chloride 1,1,2,2-Tetrachloroethane Tetrachloroethylene Toluene 1,1,1-Trichloroethane 1,1,2-Trichloroethane Trichloroethylene	0.002 0.002	<pre>&lt;0.002 &lt;0.002 re>
Trichlorofluoromethane Vinyl chloride m,p-Xylene o-Xylene	0.002 0.002 0.002 0.002	<0.002 <0.002 <0.002 <0.002

Lab Number Sample I.D. Clients Job Number	070590-2D 2314-Travel blank WESA P.O.#17774	
DETERMINATION	DETECTION (mg/L)	RESULTS (mg/L)
Benzene	0.002	<0.002
Bromodichloromethane	0.002	<0.002
Bromoform	0.002	0.004
Bromomethane	0.002	<0.002
Carbon tetrachloride	0.002	0.005
Chlorobenzene	0.002	<0.002
Chloroethane	0.002	<0.002
2-Chloroethylvinyl ether	0.002	<0.002
Chloroform	0.002	<0.002
Chloromethane	0.002	<0.002
Dibromochloromethane	0.002	<0.002
1,2-Dichlorobenzene	0.002	<0.002
1,3-Dichlorobenzene	0.002	<0.002
1,4-Dichlorobenzene	0.002	<0.002
1,2-Dichloroethane	0.002	<0.002
1,1-Dichloroetane	0.002	<0.002
1,1-Dichloroethylene	0.002	<0.002
trans-1,2-Dichloroethylene	0.002	<0.002
1,2-Dichloropropane	0.002	<0.002
cis-1,3-Dichloropropene	0.002	<0.002
trans-1,3-Dichloropropene	0.002	<0.002
Ethylbenzene	0.002	<0.002
Methylene chloride	0.002	<0.002
1,1,2,2-Tetrachloroethane	0.002	<0.002
Tetrachloroethylene	0.002	<0.002
Toluene	0.002	<0.002
1,1,1-Trichloroethane	0.002	<0.002
1,1,2-Trichloroethane	0.002	<0.002
Trichloroethylene	0.002	<0.002
Trichlorofluoromethane	0.002	<0.002
Vinyl chloride	0.002	<0.002
m,p-Xylene	0.002	<0.002
o-Xylene	0.002	<0.002

Lab Number Sample I.D. Clients Job Number	070590-2B 2314-TW1-48HR. WESA P.O.#17773	3
DETERMINATION	DETECTION (mg/L)	RESULTS (mg/L)
Benzene	0.002	<0.002
Toluene	0.002	<0.002
Ethylbenzene	0.002	<0.002
m,p-Xylene	0.002	<0.002
o-Xylene	0.002	<0.002

### WATER QUALITY ANALYSIS

### ARECO CANADA INC. 28 CONCOURSE GATE, NEPEAN, ONTARIO K2E 7T7

Lab. Number Sample I.D. Clients Job Number	070590-2B 2314-TW1-48HR. WESA P.O.#17773	<b>;</b>
DETERMINATION	DETECTION	RESULTS

DETERMINATION	DETECTION	RESULTS
Colour (true) Hardness (CaCO <sub>3</sub> ) Alkalinity (CaCO <sub>3</sub> ) Turbidity Conductivity pH Chloride Fluoride Sulphate Nitrate (N) Nitrite (N) Calcium Sodium Ammonia (N) Potassium Iron Manganese Magnesium Hydrogen sulphide Phenols Total Nitrogen (TKN) Tannin/Lignin TOC DOC BOD Silica Coliform Count Fecal Count Fecal Strept. Background Uranium	1.0 TCU 0.05 mg/l 1.0 mg/l 1.0 NTU uS/cm 0.00 units 0.01 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.05 mg/l 0.07 mg/l 0.08 mg/l 0.09 mg/l 0.09 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.00 mg/l 0.1 mg/l 1 mg/l 1 mg/l 1 mg/l 1 mg/l 0.01 mg/l 0.015 mg/l per 100 ml per 100 ml per 100 ml per 100 ml	25 - - 5 - - - 0.741 - 0.008* unpreserved
Cation Sum Anion Sum % Difference Ion Ratio TDS (ion sum calculated) Conductivity (calc.) SAR	meq/l meq/l % mg/l umho/cm	

TABLE 5, DRINKING WATER ANALYSIS

ARECO CANADA INC., 28 CONCOURSE GATE, NEPEAN, ONTARIO, K2E 7T7

 Lab Number
 070590-2C

 Customer I.D.
 2314-TW1-72HR.

 Clients Job Number
 P.O.# 17774

TABLE 1: Parameters Related to Health

PARAMETER	M.O.E. GUIDELINES	DETECTION LIMITS	RESULTS
Arsenic (ppm) Barium (ppm) Boron (ppm) Cadmium (ppm) Chromium (ppm) Cyanide (ppm) Fluoride (ppm) Lead (ppm) Mercury (ppm) Nitrate(N) (ppm) Nitrite(N) (ppm)	0.05 1.0 5.0 0.005 0.05 0.2 2.4 0.05 0.001 10.0 1.0	0.005 0.002 0.005 0.001 0.001 0.02 0.05 0.005 0.001 0.05 0.05	<0.005 0.009 0.010 <0.001 <0.001 <0.02 <0.05 <0.005 <0.001 0.10 <0.05 <0.02
Pesticides			
Aldrin (ppb) Dieldrin (ppb) Carbaryl (ppb) Chlordane (ppb) DDT (ppb) Diazinon (ppb) Endrin (ppb) Heptachlor (ppb) Hep. epoxide (ppb) Lindane (ppb) Methoxychlor (ppb) Methyl Parathion (ppb) Parathion (ppb) Toxaphene (ppb) 2,4-D (ppb) 2,4,5-TP	0.7 0.7 70 7 30 14 0.2 3 3 4 100 7 35 5 100 10	0.1 0.05 0.02 0.04 0.03 0.4 0.02 0.1 0.1 0.001 0.02 0.2 0.3 5 0.3 0.2	<0.1 <0.05 <0.02 <0.4 <0.03 <0.4 <0.02 <0.1 <0.001 <0.02 <0.2 <0.2 <0.3 <4

TABLE 1 continued...

### Radionuclides (Becquerels/Litre)

Tritium Cobalt-60 Strontium-90 Iodine-131 Cesium-134 Cesium-137 Radium-226	- - - - - -	100 1 1 1 1 1 0.1	<100 <1 <1 <1 <1 <1 <1 <1 <1
Trihalomethanes (ppm)			
Chloroform Dichlorobromomethane Chlorodibromomethane Bromoform	0.35	0.002	<0.002
	0.35	0.002	<0.002
	0.35	0.002	<0.002
	0.35	0.002	<0.002
Selenium (ppm)	0.01	0.005	<0.005
Silver (ppm)	0.05	0.001	<0.001
Turbidity (FTU)	1	1	5

TABLE 2: Parameters Related to Aesthetic Quality

PARAMETER	M.O.E. GUIDELINES	DETECTION LIMITS	RESULTS
Chloride (ppm) Colour (TCU)	250 5	0.01	3.79 23
Copper (ppm)	1.0	0.001	<0.001
Iron (unfiltered) (ppm		0.002	0.731
Iron (filtered)	0.3	0.002	0.008
Manganese (ppm)	0.05	0.001	0.001
Methane (ppm)	$3 L/m^3$	0.01	0.981
Odour	Inoffensive	-	Inoff.
Organic Nitrogen (ppm)		0.05	<0.05
Phenols (ppm)	0.002	0.002	<0.002
Sulphate (ppm)	500	0.02	3.53
<b>*</b>	Inoffensive	0.006	0.066
Taste	Inoffensive	_	Inoff.
TDS (caculated)	500		477
TOC (ppm)	5.0	T.0	5
Zinc (ppm)	5.0	0.001	0.002

#### FASCIMILE MESSAGE

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Sample I.D. Clients Job Number	070590-2C 2314-TW1-72HR. WESA P.O.#17774	4
DETERMINATION	DETECTION (mg/L)	RESULTS (mg/L)
Benzene	0.002	<0.002
Bromodichloromethane	0.002	<0.002
Bromoform	0.002	<0.002
Bromomethane	0.002	<0.002
Carbon tetrachloride	0.002	<0.002
Chlorobenzene	0.002	<0.002
Chloroethane	0.002	<0.002
2-Chloroethylvinyl ether	0.002	<0.002
Chloroform	0.002	<0.002
Chloromethane	0.002	<0.002
Dibromochloromethane	0.002	<0.002
1,2-Dichlorobenzene	0.002	<0.002
1,3-Dichlorobenzene	0.002	<0.002
1,4-Dichlorobenzene	0.002	<0.002
1,2-Dichloroethane	0.002	<0.002
1,1-Dichloroetane	0.002	<0.002
1,1-Dichloroethylene	0.002	<0.002
trans-1,2-Dichloroethylene	0.002	<0.002
1,2-Dichloropropane	0.002	<0.002
cis-1,3-Dichloropropene	0.002	<0.002
trans-1,3-Dichloropropene	0.002	<0.002
Ethylbenzene	0.002	<0.002
Methylene chloride	0.002	<0.002
1,1,2,2-Tetrachloroethane	0.002	<0.002
Tetrachloroethylene	0.002	<0.002
Toluene	0.002	<0.002
1,1,1-Trichloroethane	0.002	<0.002
1,1,2-Trichloroethane	0.002	<0.002 <0.002
Trichloroethylene	0.002	<0.002
Trichlorofluoromethane	0.002 0.002	<0.002
Vinyl chloride	0.002	<0.002
m,p-Xylene o-Xylene	0.002	<0.002

TABLE 5, DRINKING WATER ANALYSIS

ARECO CANADA INC., 28 CONCOURSE GATE, NEPEAN, ONTARIO, K2E 7T7

Lab Number 070590-2C
Customer I.D. 2314-TW1-72HR.
Clients Job Number P.O.# 17774

TABLE 1: Parameters Related to Health

PARAMETER	M.O.E. GUIDELINES	DETECTION LIMITS	RESULTS
Arsenic (ppm) Barium (ppm) Boron (ppm) Cadmium (ppm) Chromium (ppm) Cyanide (ppm) Fluoride (ppm) Lead (ppm) Mercury (ppm) Nitrate(N) (ppm) Nitrite(N) (ppm)	0.05 1.0 5.0 0.005 0.05 0.2 2.4 0.05 0.001 10.0 1.0	0.005 0.002 0.005 0.001 0.001 0.02 0.05 0.005 0.001 0.05 0.05	<0.005 0.009 0.010 <0.001 <0.002 <0.05 <0.005 <0.005 <0.005 <0.05 <0.05
Pesticides			
Aldrin (ppb) Dieldrin (ppb) Carbaryl (ppb) Chlordane (ppb) DDT (ppb) Diazinon (ppb) Endrin (ppb) Heptachlor (ppb) Hep. epoxide (ppb) Lindane (ppb) Methoxychlor (ppb) Methyl Parathion (ppb) Parathion (ppb) Toxaphene (ppb) 2,4-D (ppb) 2,4,5-TP	0.7 0.7 70 7 30 14 0.2 3 3 4 100 7 35 5	0.1 0.05 0.02 0.04 0.03 0.4 0.02 0.1 0.1 0.001 0.02 0.2 0.3 5	<0.1 <0.05 <0.02 <0.4 <0.03 <0.4 <0.02 <0.1 <0.001 <0.02 <0.2 <0.2 <0.3 <4

TABLE 1 continued ...

### Radionuclides (Becquerels/Litre)

Tritium	-	100	<100
Cobalt-60	444	1	<1
Strontium-90	<del></del>	1	<1
Iodine-131	_	1	<1
Cesium-134	<del>-</del>	1	<1
Cesium-137	name .	1	<1
Radium-226	«24%	0.1	<1
Trihalomethanes (ppm)			
Chloroform	0.35	0.002	<0.002
Dichlorobromomethane	0.35	0.002	<0.002
Chlorodibromomethane	0.35	0.002	<0.002
Bromoform	0.35	0.002	<0.002
Selenium (ppm)	0.01	0.005	<0.005
Silver (ppm)	0.05	0.001	<0.001
Uranium (ppb)		0.1	<0.1
Turbidity (FTU)	1	1	5

TABLE 2: Parameters Related to Aesthetic Quality

PARAMETER	M.O.E. GUIDELINES	DETECTION LIMITS	RESULTS
Chloride (ppm)	250	0.01	3.79
Colour (TCU)	5	1	23
Copper (ppm)	1.0	0.001	<0.001
Iron (unfiltered) (ppm	0.3	0.002	0.731
Iron (filtered)	0.3	0.002	0.008
Manganese (ppm)	0.05	0.001	0.001
Methane (ppm)	3 L/m <sup>3</sup>	0.01	0.981
Odour	Inoffensive	-ma	Inoff.
Organic Nitrogen (ppm)	0.15	0.05	<0.05
Phenols (ppm)	0.002	0.002	<0.002
Sulphate (ppm)	500	0.02	3.5 <b>3</b>
Sulphide	Inoffensive	0.006	0.066
Taste	Inoffensive	<del></del>	Inoff.
TDS (caculated)	500		477
TOC (ppm)	5.0	1.0	5
Zinc (ppm)	5.0	0.001	0.002

project 2314

## 900536 Water Earth & Science

CONCENTRATION OF VOLATILE PRIORITY POLLUTANTS IN VATER ug/L

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## ARECO CANADA INC.

APPLIED RESEARCH DIVISION

28 CONCOURSE GATE NEPEAN, ONTARIO CANADA K ZE 777 TEL. (613) 228-1145 FAX. (613) 228-1148

CUSTOMER: WATER & EARTH SCIENCE ASSOCSTOMER REF. #:

ATTN: TAMI SUGARMAN ORDER REF. #: 2314

REPORT #: 3352905

SAMPLE RECEIVED: MAY 28/90

DATE SUBMITTED: MAY 29/90

CERTIFICATE OF ANALYSIS

SAMPLE DESCRIPTION:

WATER

ANALYSIS PERFORMED:

Fe

**INSTRUMENTATION:** 

IC

**RESULTS:** 

See attached

CERTIFIED BY: Greg Clarkin

WATER QUALITY ANALYSIS

ARECO CANADA INC., 28 CONCOURSE GATE, NEPEAN, ONTARIO K2E 7T7

Lab Number Sample I.D. Clients Job Number	280590-5 Vars Water Supply # 2314	
SAMPLE DESCRIPTION	RESULTS Fe (ppm)	
2314-1hr. 2314-6hrs. 2314-12hrs. 2314-48hrs. 2314-72hrs.	0.395 0.260 0.278 0.233 0.240	Market State Control

_AB	REPOR	TNO	).:	A0-0766
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## **REPORT OF ANALYSES**

Client:	Water	&	Earth	Science	Assoc.	Ltd.	Date:	May	15,	1990
		•••								
	Attn:	Ms	. Tami	. Sugarma	an		Project:	2314	+	

		Sample	Sample	Sample	Sample	Sample
Parameter	Units			A Marian		The second secon
Fe	mg/L	0.67				
Mn	mg/L					
Hardness	mg/L CaCO <sub>3</sub>					
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pН					No.	
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# Numéro d ACCUTEST Laboratories Ltd. 146 Colonnade Road, Suite 202, Nepean, Ontario K2E 7Y3 (613) 727-5692

Numéro de rapport: A0 - 076 6

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# APPENDIX E Correspondence

Ministry of the Environment

Mailing Address PO Box 820 Kingston Ontario K7L 4X6 Adresse postale C.P. 820 Kingston (Ontario) K7L 4X6 133 Daiton Avenue Kingston Ontario K7K 6C2 613 549-4000 133. avenue Dalton Kingston (Ontario) K7K 6C2 613 549-4000

2 May 1990

Water and Earth Science Associates Limited Box 430 CARP, Ontario KOA 120

Attention: Tami Sugarman

#### Dear Madam:

Re: Approval to Take Water Under Section 20 of the Ontario Water Resources Act as Requested by Your Application Dated April 30, 1990

Communal Test Well, Lots 26 and 27, Concession V Cumberland Township

Test start date: May 3rd, 1990
Type : Pumping Test
Rate : 350 IGPM
Duration : Three Days

This letter constitutes approval to take water under Section 20 of the Ontario Water Resources Act. This approval is subject to the following conditions:

- 1) The pumping rate and period of pumping must not exceed the total water withdrawal requested without the approval of this Ministry.
- 2) All supply wells within 300 metres of the test well shall be located and monitored for water quality and water levels prior to test pumping. Water level drawdown during pumping and recovery after pumping shall also be monitored.

The well owners must be contacted and permission obtained to access their well at least 10 days prior to the test pumping. If the owner agrees, water level and quality sampling shall be carried out. The accessibility of the well is the responsibility of the owner. If the owner does not agree to the testing, the owner's refusal should be recorded.

- 3) All well supply water and surface discharge problems associated with the testing must be reported to this Ministry.
- 4) All water supplies adversely affected during the testing must be replaced with temporary water supplies until the testing has been completed and/or the affected water supplies are restored.
- 5) A report of the pumping test must be submitted to this Ministry.
- 6) When the water taken is discharged to a watercourse, the quality and temperature of the groundwater shall be substantially the same as the receiving stream to ensure that the stream's water quality, flora and fauna are not adversely affected by the discharge. If the rate of discharge is substantial, energy absorbing padding shall be used to prevent erosion. The rate of discharge shall be controlled to prevent downstream flooding and property damage.
- 7) The Ministry of the Environment must be advised of any intent to abandon the test well.
- 8) If the test well is abandoned or not used for any extended period of time, it shall be properly sealed to prevent any groundwater contamination.

The testing shall be carried out under these general conditions. The reason for the imposition of these conditions is to ensure that the water quality and quantity of all surface water, groundwater and water supplies in the area of the testing are protected.

You may, by written notice served upon me and the Environmental Appeal Board within 15 days after receipt of this approval, require a hearing by the Board. Section 63 of the Ontario Water Resources Act, as amended in 1983, provides that the Notice requiring the hearing shall state the portions of each Term or Condition in the approval in respect of which the hearing is required and the grounds on which you intend to rely at the hearing.

This approval is for the temporary taking only (3 days). If the well is put into service for an extended period of time, a Permit to Take Water will be required if the taking is in excess of 50,000 litres per day. This approval does not release you from

any legal liability or obligation imposed by law and should not be construed as limiting any legal claims or rights of action that any person, including the Crown in Right of Ontario or any agency thereof, has or may have against you, your officers, employees, agents and your contractors.

Yours truly,

M.M. Holy, Chief

Approvals and Planning Technical Support Section Southeastern Region

PLS/sh

#### TELECOPIER COVER SHEET

#### MINISTRY OF THE ENVIRONMENT

133 Dalton Avenue KINGSTON, Ontario

то:	Jan	<u>-i Su</u>	ganno	<u> </u>			
FROM:	Fra	ak Cros	sley				
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IF YOU DO NOT RECEIVE THE TOTAL NUMBER OF PAGES SPECIFIED, OR IF YOU HAVE TROUBLE READING THE COPY, PLEASE CALL THE FOLLOWING NUMBER FOR ASSISTANCE.

TELEPHONE: (613) 549-4000

CONTACT: Mrs. C. Bishop

Contact - Phone call 1:30 pm May 3,1990
Penny Swelight - MOE

message from F. Crossley: if you follow these quidelies + comments of letter of March 23/88 you should be fire with respect to ministy of environ requireneds.

Reaeved by T. Sugarna

# Ministry of the Environment Southeastern Region

#### Draft Copy

#### GUIDELINES FOR APPLICANTS TO THE APPROVALS AND PLANNING UNIT:

PUMPING TESTS
AND THE DETERMINATION OF WATER QUALITY
IN COMMUNAL WELLS

April, 1990

#### Objective

These guidelines relate to the establishment of the suitability of a well as a communal water supply. Site-specific characteristics not covered by these guidelines should also be addressed by the consultant. In general, it is up to the consultant to show that a well is capable of supplying sufficient water of acceptable quality on a long-term basis.

Note: Proponents of a communal water supply project should be advised that the project will probably require a <u>Water Works Certificate of Approval</u> (see section entitled "Legislation", below). Separate guidelines pertaining to various types of Water Works are available from the Approvals and Planning Unit. These guidelines may have a bearing on how the pumping tests and water quality determinations are carried out, and should therefore be used in conjunction with the present guidelines.

#### Well Hydraulics

Pumping tests should be carried out by a competent hydrogeological consultant.

Each pumping test should include:

- a preliminary step pumping test to determine an appropriate rate for the constant rate pumping test.

. . . . . 2

The last sampling should occur shortly before the end of the pumping test. This sample should be submitted to a qualified laboratory for analysis with respect to <u>all</u> of the Provincial Drinking Water Quality Objectives (refer to the Ministry of the Environment's "blue book": <u>Water Management: Goals</u>, <u>Policies</u>, <u>Objectives and Implementation Procedures of the Ministry of the Environment</u>, published 1978, revised 1984).

The hydrogeological consultant should establish the compliance of the proposed groundwater supply with the Provincial Drinking Water Quality Objectives. The consultant should also comment on any trends in the water quality data. The possibility of changes in water quality with time and with changes in the pumping rate should be considered with reference to the Drinking Water Objectives.

#### Legislation

The proponent should be informed that the Ministry of the Environment may require the following under the Ontario Water Resources Act:

- a <u>Water Works Approval</u> under Section 23 of the Act (refer to the Act to determine whether the characteristics of the water supply system make it subject to this requirement).
- a <u>Permit To Take Water</u> under Section 20 of the Act. The <u>Permit</u> would be required for the taking of more than a total of 50,000 litres in any 24-hour period for certain purposes, including pumping tests. Under the terms and conditions of this Permit, the proponent would be required to restore groundwater supplies that have been seriously interfered with.

C.Hammond
/mz

- the constant rate pumping test, starting from static water level conditions. Its duration should be a minimum of twenty-four hours. The pumping rate should deviate no more than 5% from the rate decided upon. Water levels should be monitored in the test well and any observation wells at a decreasing frequency best suited to provide a smooth fit on semi-log graph paper. During the pumping test waste water should be discharged at an appropriate distance from the test well to ensure artificial recharge does not occur.
- the monitoring of water level recovery, starting immediately after the pumping test. The recovery should be monitored in the test wells until 95% recovery of the original static water level conditions occurs. Recovery water levels should be monitored at a decreasing frequency best suited to provide a smooth fit on semilog graph paper.

Using the data from the pumping and recovery tests the consultant should be able to assess with confidence the direction of groundwater flow, the aquifer's hydraulic properties, sustainable long term yields, the effect of interacting pumping cones of influence (in the case where more than one well is proposed), and the potential for interference with other water supplies in the area.

#### Water Ouality

Chemical and bacteriological water quality sampling should be conducted at least twice during the pumping test to establish the potability of groundwater supplies. The first sampling should occur shortly after the beginning of the pumping test. This first sample should be submitted to a qualified laboratory for analysis for the following water quality parameters:

bacteriological - total coliform, fecal coliform, fecal streptococci and background;

chemical - hardness, alkalinity, iron, chloride, pH,
fluoride, conductivity, sodium, calcium, potassium,
magnesium, ammonia, total Kjeldahl nitrogen, nitrate,
nitrite, sulphate, phenols and hydrogen sulphide gas.

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#### APPENDIX F

Theoretical Aquifer Yield and Well Interference Calculations

#### THEORETICAL AQUIFER YIELD AND WELL INTERFERENCE CALCULATIONS

#### Theoretical Aquifer Yields

The theoretical aquifer yield can be calculated using the following formula:

$$Q_{max} = \frac{4\pi T \Delta smax}{W(u)}$$
 where  $Q_{max} = maximum discharge [m^3/day]$ 
 $T = transmissivity [m^2/day]$ 
 $\Delta smax = maximum allowable drawdown [m]$ 
 $W(u) = well function [N]$ 

The well function is derived by means of well function tables that are based on the following:

$$u = \frac{r^2S}{4Tt}$$
 where  $r = radial$  distance from pumping well [m]  $S = storativity$  [N]  $t = time since pumping began [days]$ 

Tests done on the test well revealed the following aquifer parameters:

$$T = 1000 \text{ m}^2/\text{day}$$
  $S = 0.0015$   $\Delta \text{smax} = 13 \text{ m}$ 

For a 10 year design period the calculations are:

$$u = \frac{(0.1)^{2}(0.0015)}{4(1000)(3650)}$$

$$= 1.03 \times 10^{-12}$$

$$W(u) = 27.0$$

$$Q_{\text{max}} = \frac{4\pi (1000)(13)}{27.0} = 6050 \text{ m}^3/\text{day} = 924 \text{ IGPM}$$

For a 20 year design period the calculations are:

$$u = \frac{(0.1)^2 (0.0015)}{4 (1000) (7300)} = 5.14 \times 10^{-13}$$

$$W(u) = 27.72$$

$$Q_{\text{max}} = \frac{4\pi (1000) (13)}{27.72}$$
$$= 5893 \text{ m}^3/\text{day}$$
$$= 900 \text{ IGPM}$$

#### Well Interference

The same equations used to calculate aquifer yield can also be used to determine theoretical well interference data. Here, however, Q is kept constant and the drawdown is calculated for a 10 year time span.

The aquifer parameters of transmissivity and storativity have been shown to be

$$T = 1000 \text{ m}^2/\text{day}$$
  $S = 1.5 \text{ x } 10^{-3}$ 

Example calculation

$$= 2.57 \times 10^{-5}$$

Therefore W(u) = 9.99

$$\Delta s = \frac{Q W(u)}{4\pi T}$$

$$= \frac{982(9.99)}{4\pi(1000)}$$

$$= 0.78 \text{ m}$$

radius(	m) u	W(u)	150 IGPM	300 IGPM
100	$1.03 \times 10^{-6}$	13.19	1.03	2.06
500	$2.57 \times 10^{-5}$	9.99	0.78	1.56
1000	$1.03 \times 10^{-4}$	8.60	0.67	1.34



### **REPORT OF ANALYSES**

Client: Water & Earth Science Associates Ltd	à	Date: N	May 30, 1990	
Attention: T. Sugarman		Project:	Vars water	supply
			2314	

		Sample	Sample	Sample	Sample	Sample
Parameter	Units	2314-1 hr	2314-6 hr	2314-12 h	r 2314-48h	: 2314-72hr
Fe (tot)	mg/L	0.69	0.73	0.73	0.72	0.72
Mn	mg/L	AND THE PROPERTY OF THE PROPER				
Hardness	mg/L CaCO <sub>3</sub>					
Alkalinity	mg/L CaCO <sub>3</sub>					
рН						
Conductivity	umhos					
F	mg/L					
Na	mg/L					
N-NO <sub>3</sub>	mg/L					
N-NO <sub>2</sub>	mg/L					
N-NH <sub>3</sub>	mg/L					
SO₄	mg/L					
CL	mg/L					
Phenols	mg/L					
Turbidity	NTU					
Colour	Pt/Co Units					
Ca	mg/L					
Mg	mg/L					
Tannin & Lignin	mg/L					
Total Nitrogen	mg/L					
К	mg/L					
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ANALYST: